



SAFE SEPARATION

Recommended Practice for Safe Wellbore
Positioning, Separation & Surveying

2026 MARCH 05 – AADE HOUSTON MEETING

AADE
AMERICAN ASSOCIATION
of DRILLING ENGINEERS

Presentation Background

Recommended Practice for Safe Well Positioning, Separation, and Surveying

Jonathan Dale Lightfoot



Society of Petroleum Engineers
Distinguished Lecturer Program
www.spe.org/dl



AADE-23-NTCE-073

Introduction to API RP 78, *Wellbore Surveying and Positioning*

Jonathan D. Lightfoot and Will Tank, Oxy; Ben Coco, API



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Abstract

The American Petroleum Institute (API) recently undertook the development of a document called Recommended Practice 78, *Wellbore Surveying and Positioning*, (RP 78), a modern technical industry standard for wellbore placement that can be applied to all wellbore construction applications. The standard is intended to serve as the primary technical reference for proven engineering practices in the applications of oil and gas, geothermal, carbon sequestration, coalbed methane (CBM), horizontal directional drilling (HDD) trenchless boring, mineral ventilation and extraction, scientific coring, and all other subsurface borehole construction applications.

API RP 78's development was led by a group of independent consultants, industry experts, academics, and representatives from public and private energy operators. The Operator's Wellbore Survey Group (OWSG), which later became an official sub-committee of the Industry Steering

We are meeting to help develop and promote good practices in wellbore surveying necessary to support wellbore construction which enhance safety and competition. The meeting will be conducted in compliance with all laws including the antitrust laws, both state and federal. We will not discuss prices paid to suppliers or charged to customers nor will we endorse or disparage vendors or goods or services, divide markets, or discuss with whom we will or will not do business, nor other specific commercial terms, because these are matters for each company or individual to independently evaluate and determine.

Virtual meetings are now held online every other month and

SPE 2024-2025 [Distinguished Lecturer Program](#)
Technical Presentation

[AADE-23-NTCE-073: Technical Paper](#)

05 MARCH 2026

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Presentation Outline

Safe Separation

Applications

Industry Collaboration

Management Principles

Position Uncertainty Models (PUMs)

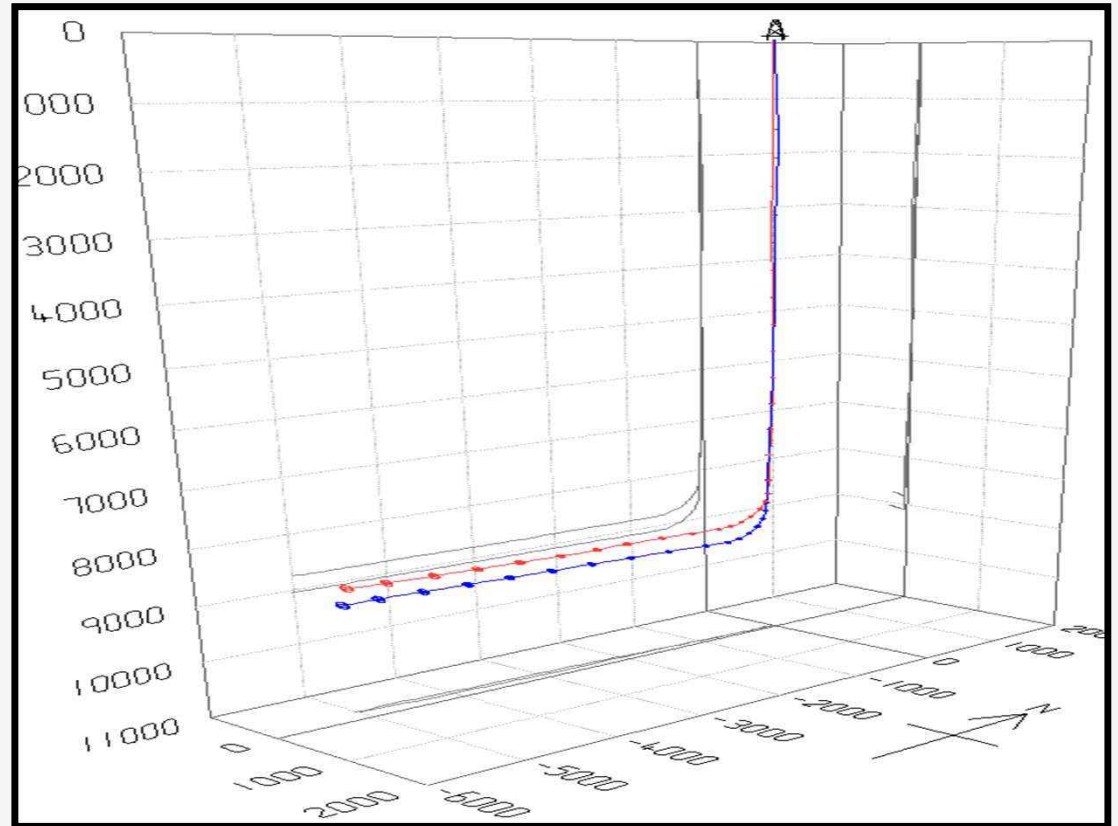
Offset Well Environment

Case Studies

- Offset Operator Close Approach
- Lateral Undulations
- Key Performance Indicators
- Steerable Motor Curve
- Lateral Tortuosity
- Texas Long Lateral Example

Key Takeaways

API RP78 Status Update



Safe Separation

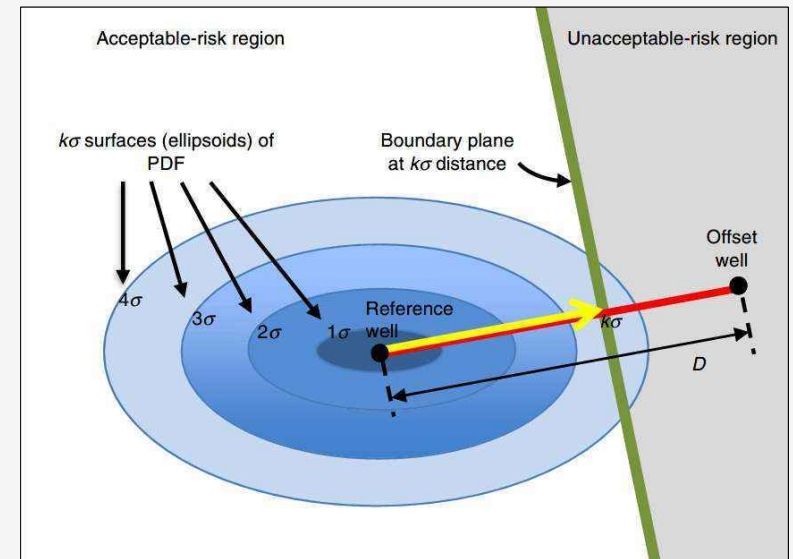
The Wellbore Positioning Technical Section (WPTS) Rule

Separation Factor = Ratio of Separation Distance and Uncertainty

$$\frac{\text{Numerator}}{\text{Denominator}} = \frac{\text{Distance}}{\text{Uncertainty}}$$

$$SF = \frac{D - R_r - R_o - S_m}{k \sqrt{\sigma_s^2 + \sigma_{pa}^2}}$$

$$\sqrt{\sigma_r^2 + \sigma_o^2} \quad k \sqrt{\sigma_s^2 + \sigma_{pa}^2}$$



Industry Collaboration

Industry Steering Committee on Wellbore Survey Accuracy

- Produces, maintains, and publishes standards for the industry
- Promotes a collaborative understanding of issues associated with wellbore surveying
- Formed in 1999, ISCWSA has been around for 29 Years [SPE 67616-PA]
- 63 General Meetings

SPE Wellbore Positioning Technical Section (WPTS)



Applications

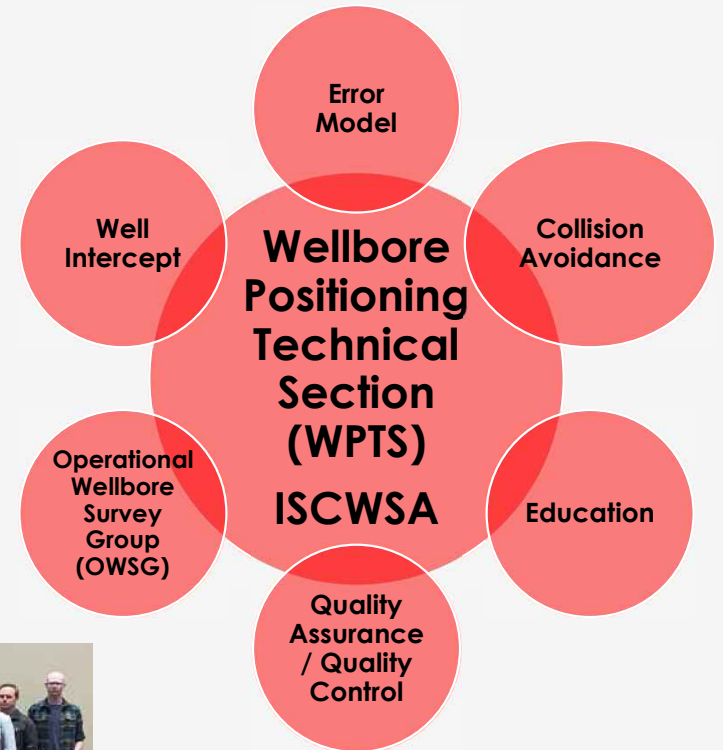
Serves as the primary technical reference for proven engineering practice in the broad wellbore construction application of:

- **Oil and Gas**
- **Geothermal**
- **Carbon Sequestration**
- **Coalbed Methane (CBM)**
- **Horizontal Directional Drilling (HDD), trenchless boring**
- **Mineral Ventilation and Extraction**
- **Scientific Coring**
- **All other subsurface borehole construction applications**

Industry Collaboration

WPTS has Six (6) Primary Sub-Committees

1. Collision Avoidance
2. Error Model Maintenance
3. Well Intercept
4. Operational Wellbore Survey Group
5. Quality Assurance / Quality Control
6. Education

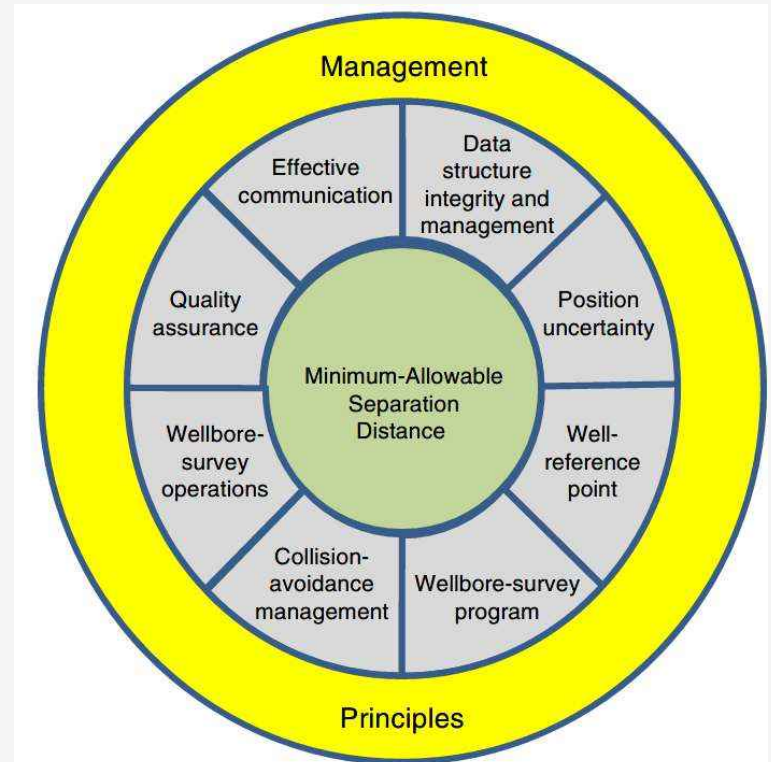
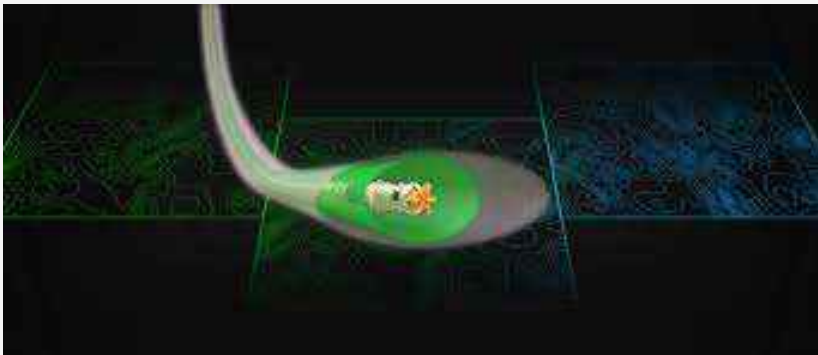


Management Principles

Minimum Allowable Separation Distance (MASD)

Maintain a Safe Separation Distance Between Wells Being Drilled and Subsurface Hazards

8 Core MASD Elements



The eight collision-avoidance elements supporting the MASD

Allowable Deviation from Plan for SF=1

Any given **separation factor (SF)** value represents a specific probability of the **reference well** crossing the **offset well**. The distance **D** at which a particular **SF** value occurs is **situation-specific**. For any point on a reference well, the critical value **SF = 1** defines a **minimum allowable separation distance (MASD)** from the specified offset well along **D**.

$$SF = \frac{D - R_r - R_o - S_m}{k \sqrt{\sigma_s^2 + \sigma_{pa}^2}}$$

$$SF = \frac{D - R_r - R_o - 0.3}{3.5 \sqrt{\sigma_s^2 + 0.25}}$$

$$k = 3.5, S_m = 0.3\text{m and } \sigma_{pa} = 0.5\text{m}$$

$$D_{MASD} = k \sqrt{\sigma_s^2 + \sigma_{pa}^2} + R_r + R_o + S_m$$

Allowable Deviation from Plan for SF=1

$$D_{MASD} = k \sqrt{\sigma_s^2 + \sigma_{pa}^2} + R_r + R_o + S_m$$

If the distance D falls below D_{MASD} , then $SF < 1$. The difference between the planned distance D_{plan} and the D_{MASD} is the allowable deviation from the plan D_{ADP} :

$$D_{ADP} = D_{plan} - D_{MASD}$$

SPE-187073-MS

Well Collision Avoidance - Separation Rule

S.J.Sawaryn, Consultant, H. Wilson, Baker Hughes a GE Company, J. Bang, Gyrodata Inc., E. Nymes, Statoil ASA, A. Sentance, Dynamic Graphics Inc., B. Poedjono and R. Lowdon, Schlumberger, I. Mitchell and J. Codling, Halliburton, P.J. Clark, Chevron Energy Technology, W.T. Allen, BP

Position Uncertainty Models (PUM)

ISCWSA & OWSG Revisions

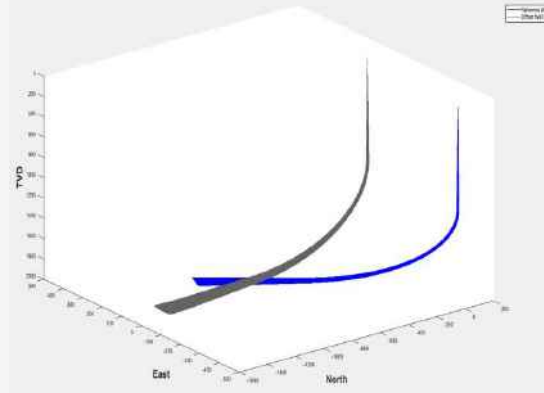
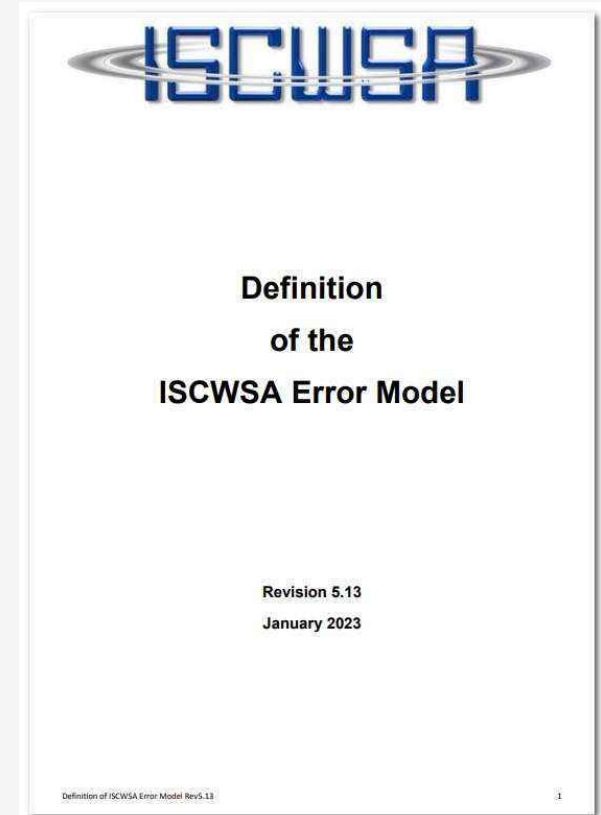
PUM Categories

Magnetic Reference Classification

Generic Models (Set A & B)

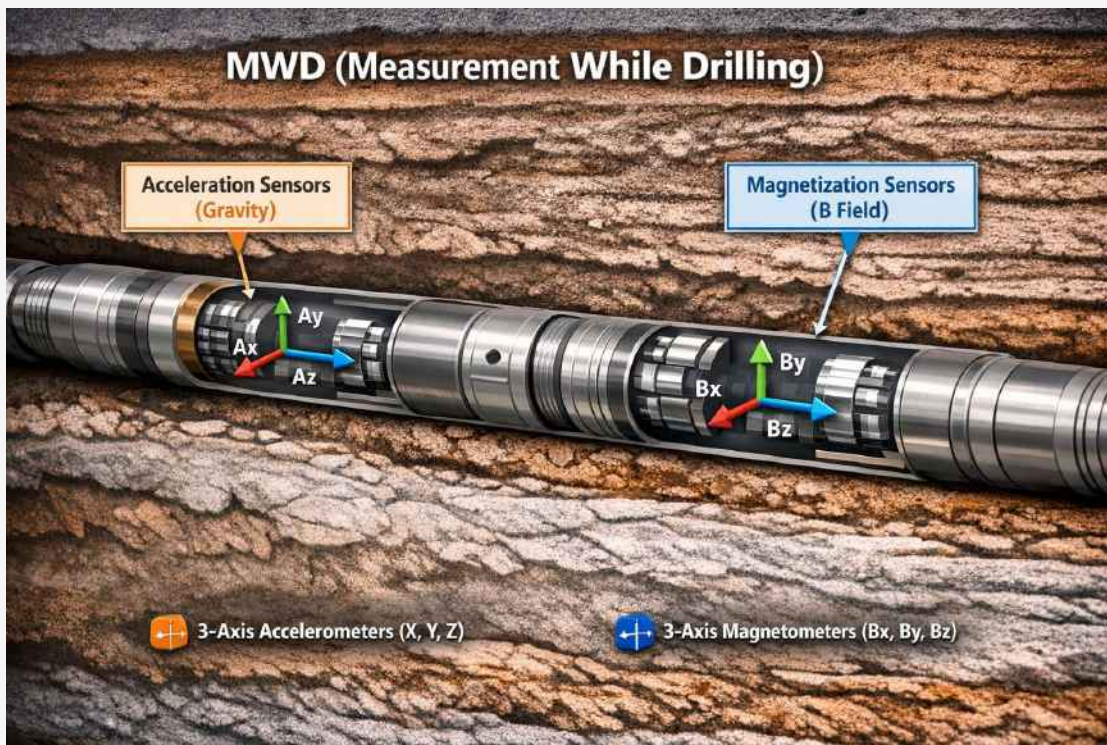
PUM Example: MWD + SRGM

MWD Corrections



MEASUREMENT WHILE DRILLING (MWD)

What does the MWD Tool Measure?



Sensor Measurements

- Acceleration
- Magnetic Field

We compute Inclination, Magnetic Azimuth, Toolface

Quality Control (Field Acceptance Criteria)

True Azimuth = Magnetic Azimuth + Declination

PUM Sets – Established by OWSG

PUM, often referred to as Error Models or Instrument Performance Models, Revision 5.13 (Current)

Set A: Standard

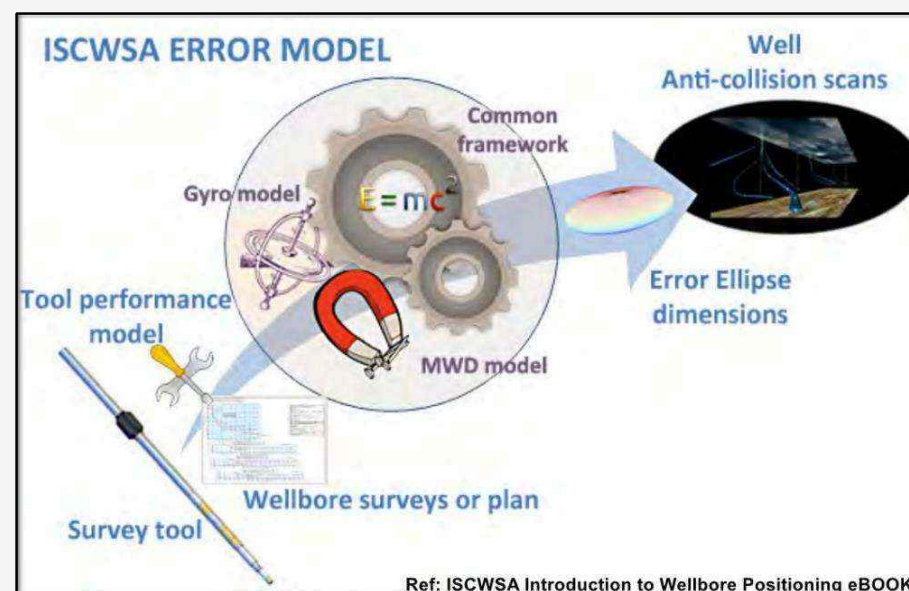
Set B: Extended

Set C: Vendor-supplied

Set D: Gyro software validation

Set E: Prototypes in development

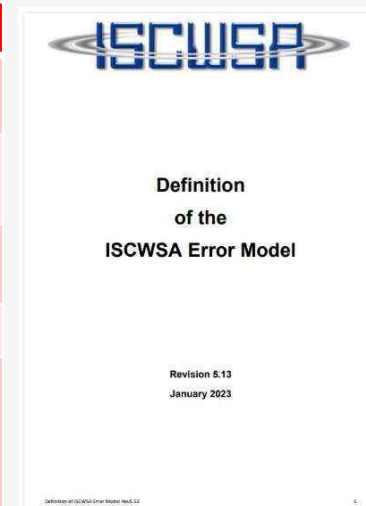
Grindrod, S. J., Clark, P. J., Lightfoot, J. D., Bergstrom, N., and L. S. Grant. "OWSG Standard Survey Tool Error Model Set for Improved Quality and Implementation in Directional Survey Management." Paper presented at the IADC/SPE Drilling Conference and Exhibition, Fort Worth, Texas, USA, March 2016.
doi: <https://doi.org/10.2118/178843-MS>



Position Uncertainty Models (PUM)



Revision	Date	Description
Rev 0	Dec 2000	As per SPE 67616 together with various typographical corrections [1]
Rev 1	March 2005	Changed to the gyro style misalignment with 4 terms and calculation options [2]
Rev 2	Feb 2007	Changes to the parameter values for the depth scale and stretch terms [2]
Rev 3	Oct 2009	Replacement of all toolface dependent terms
Rev 4 & OWSG Rev 2	Mar 2019	Introduction of AMIL term and changes to misalignment magnitudes. Random magnetic reference values introduced to the main MWD model. OWSG includes Conventional, Gyro and Utility PUMs. Included Low Resolution and High Resolution Magnetic Reference Models for MWD and EMS. [3]
Rev 5 (Beta)	Oct 2020	Introduction of the XCL term, changes to misalignments and sag, breakout of magnetic reference terms and clarification of the surface tie-on. [4]
Rev 5.13	Jan 2023	Minor updates to Rev 5 [4] – Latest Official Revision Five



1. <https://doi.org/10.2118/67616-PA>
2. <https://doi.org/10.2118/105558-MS>
3. <https://doi.org/10.2118/178843-MS>
4. <https://www.iscwsa.net/media/files/files/64bd61c2/definition-of-iscwsa-error-model-v5-13.pdf>

PUM Primary Categories

PUM
Categories

```
graph TD; A[PUM Categories] --- B[Magnetic]; A --- C[Gyro]; A --- D[Utility]
```

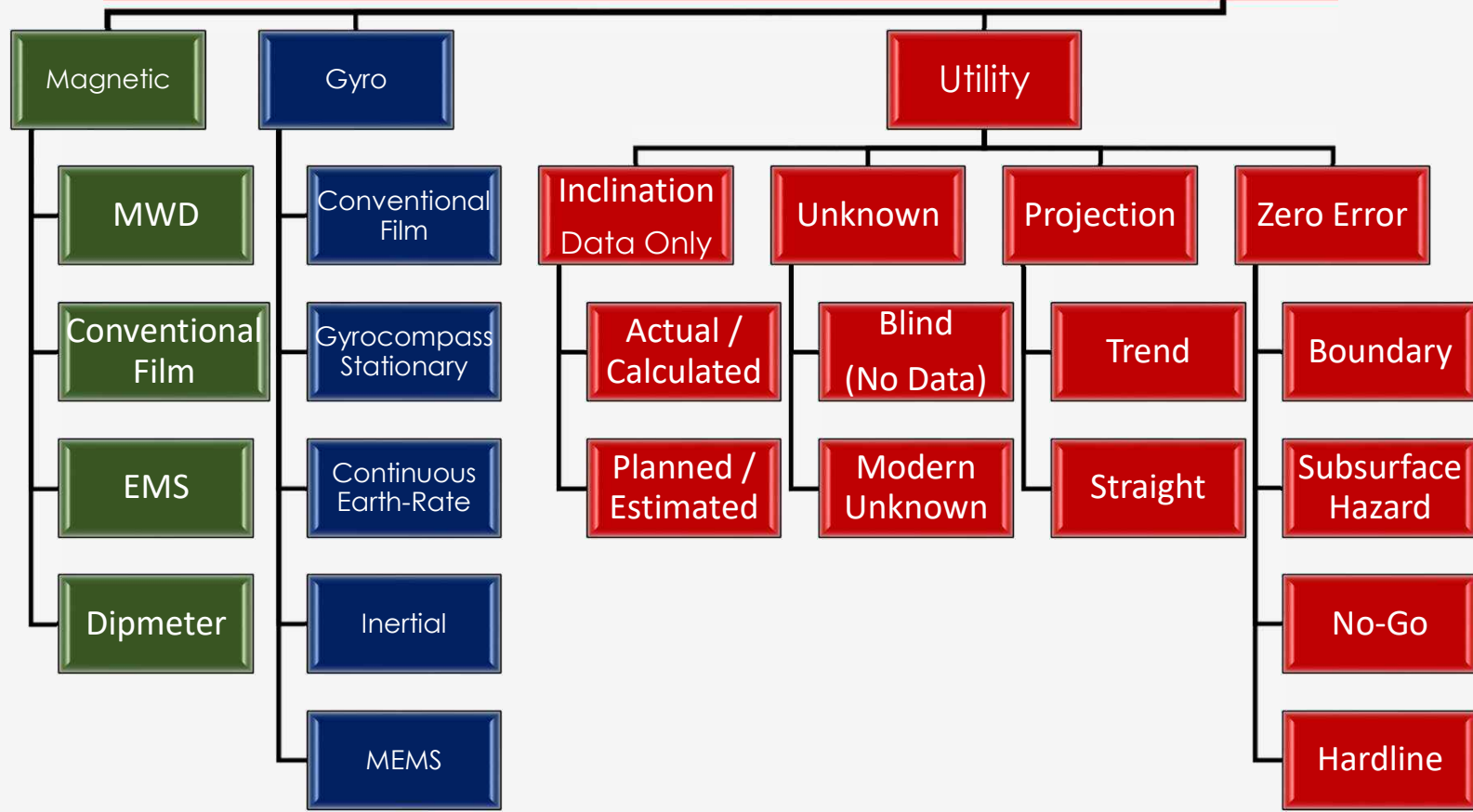
Magnetic

Gyro

Utility

PUM Categories

PUM
Categories

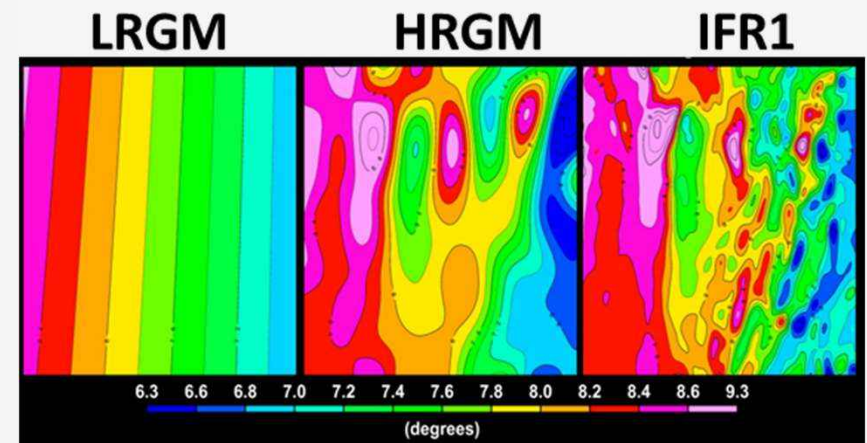
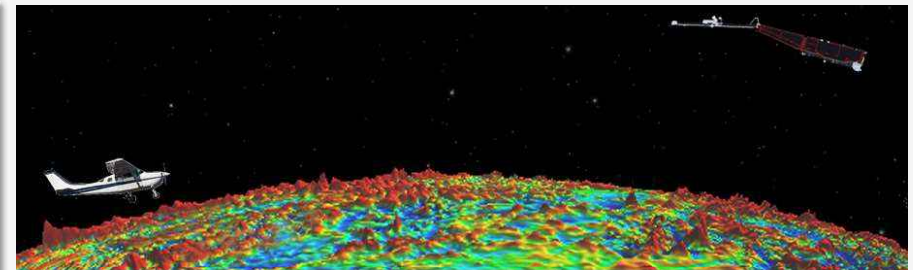
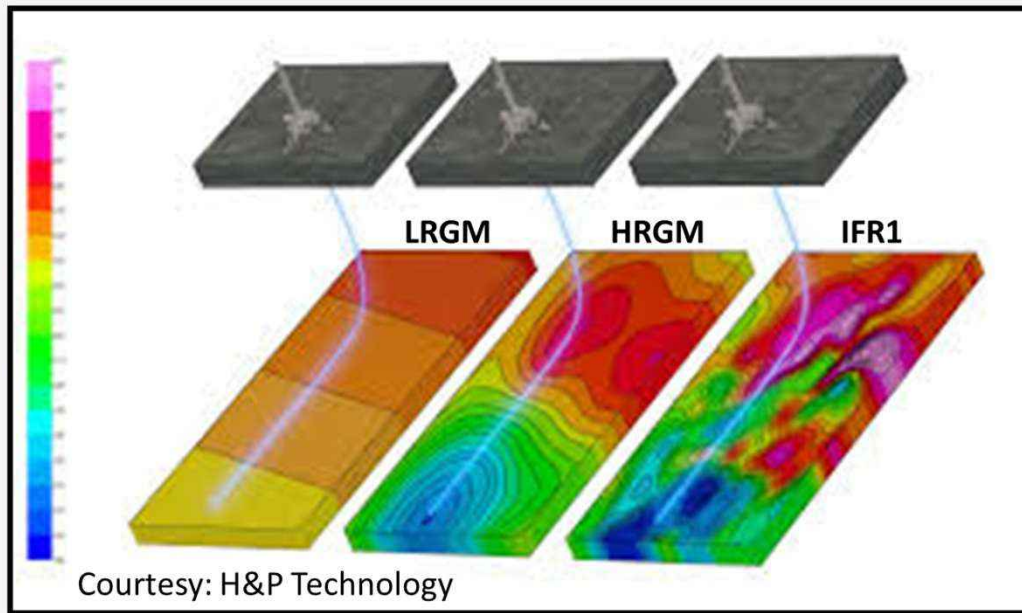


Magnetic Reference PUM Classification



Category	Abbreviation	Example Geomagnetic Models	Wavelength from 40,000 km Coverage	Update Frequency	Multiplier	Category
Low Resolution	LRGM	GRF, WMM, CGRF	≤ 4000 km	Less than Annual		
Standard Resolution	SRGM	MVSD, Pre-BGGM2019	≤ 300 km	Annual		
High Resolution	HRGM	HDGM, MVHD, BGGM2019+, HDGM-RT	≤ 55 km	Annual		
In-Field Referencing	IFR1	IFR, IFR1, Ground shot plus secular variation correction	≤ 2 km	Annual	1.21	LRGM
In-Field Referencing with Realtime Disturbance Field Correction	IFR2	IFR2, IIFR	≤ 2 km plus local realtime (≤ 1 min) sampling	Annual	1.00	SRGM
					0.82	HRGM

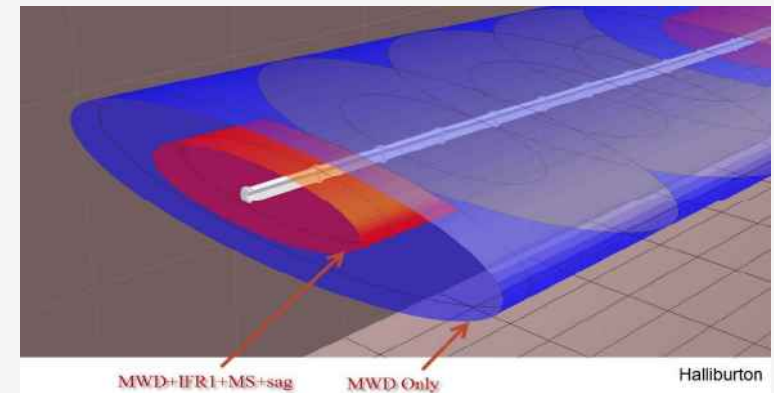
Magnetic Reference PUM Classification



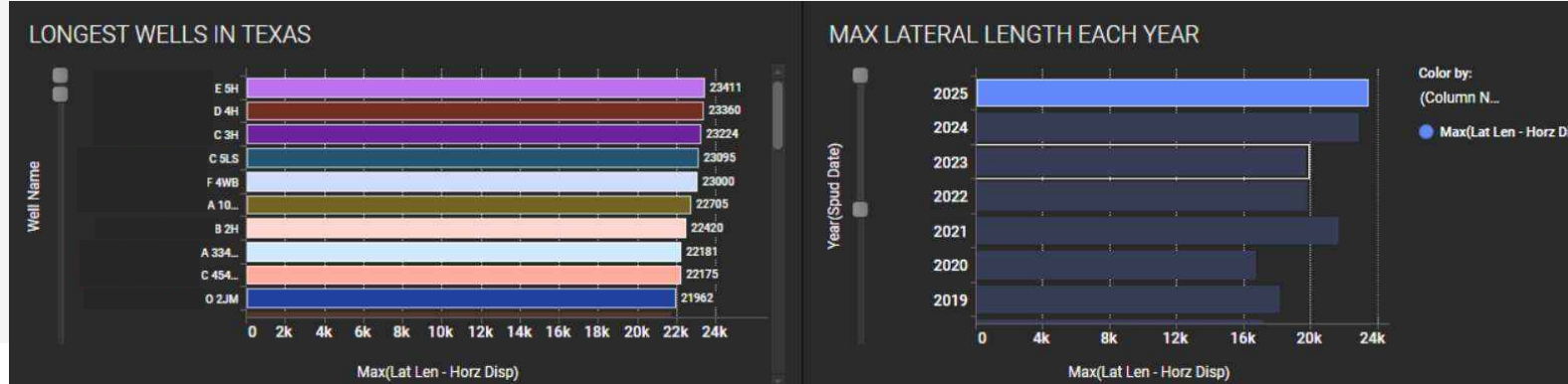
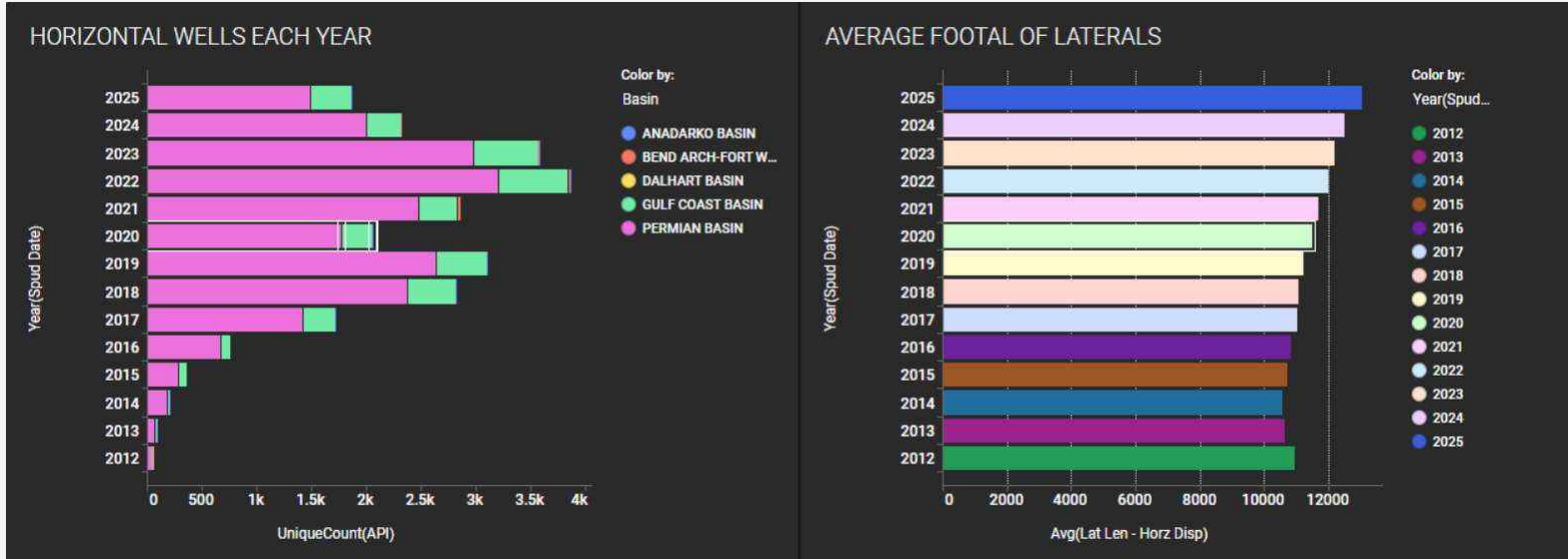
Ultra Long Laterals - Case Study

Texas: 155,759 Horizontal Wells

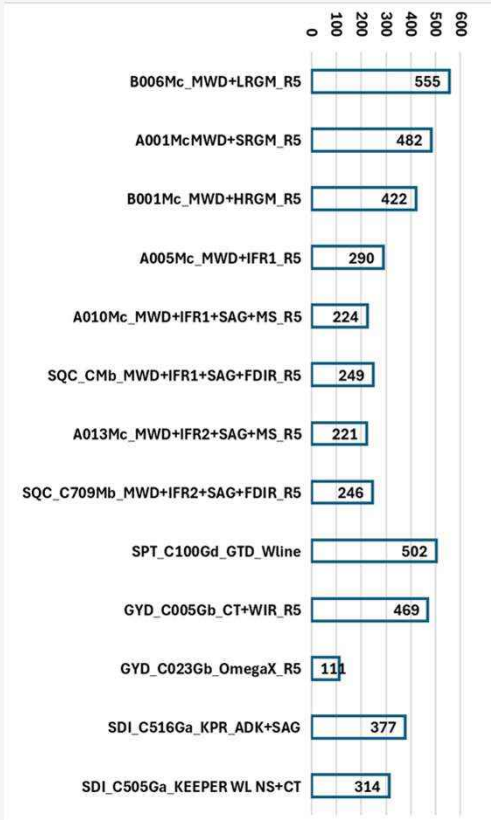
- 25,730 Laterals > 10K ft Departure
- 2216 Laterals > 15K ft Departure
- 45 Laterals > 20K ft Departure
- 5 Laterals > 23,000 ft Departure
- Longest in TX: 33,913 ft MD April 19 – June 9, 2025
 - Eagle Ford – La Salle County (API# 4229337753) – 23,411 ft Displacement



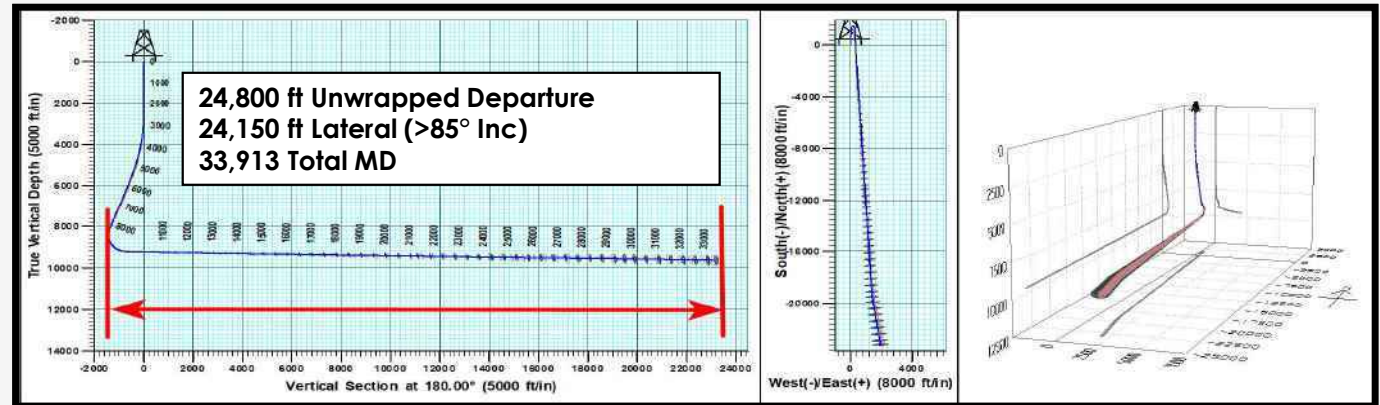
EXAMPLE – TEXAS COMPLEX WELLS



TX EXAMPLE – PUM COMPARISON



GEOMAGNETIC REFERENCE	PUM ISCWSA CODE	LATERAL UNCERTAINTY (Radius ft)	VERTICAL UNCERTAINTY (Radius ft)	LATERAL IMPROVEMENT	VERTICAL IMPROVEMENT
LRGM	B006Mc_MWD+LRGM_R5	555	253	-15%	-
SRGM	A001McMWD+SRGM_R5	482	253	REFERENCE	REFERENCE
HRGM	B001Mc_MWD+HRGM_R5	422	253	12%	-
IFR1	A005Mc_MWD+IFR1_R5	290	253	40%	-
IFR1	A010Mc_MWD+IFR1+SAG+MS_R5	224	146	53%	42%
IFR1	SQC_Cmb_MWD+IFR1+SAG+FDIR_R5	249	146	48%	42%
IFR2	A013Mc_MWD+IFR2+SAG+MS_R5	221	146	54%	42%
IFR2	SQC_C709Mb_MWD+IFR2+SAG+FDIR_R5	246	146	49%	42%
WIRELINE GYRO	SPT_C100Gd_GTD_Wline	502	108	-4%	57%
WIRELINE GYRO	GYD_C005Gb_CT+WIR_R5	469	99	3%	61%
DROP GYRO	GYD_C023Gb_OmegaX_R5	111	106	77%	58%
DROP GYRO	SDI_C516Ga_KPR_ADK+SAG	377	154	22%	39%
WIRELINE GYRO	SDI_C505Ga_KEEPER WL NS+CT	314	162	35%	36%



PUM Toolcodes Rev 5-1

A default set of conservative PUM tool-codes for use when tool specific models are not available.

[ISCWSA Generic Toolcodes SetA Rev5-1](#)
(updated Sept 23, 2022)

[ISCWSA Generic Toolcodes SetB Rev5-1](#)
(updated Sept 23, 2022)

- Header / Reference Info
- Weighting Functions
- Technical Reference / Source
- Code & Term Description
- Type, Magnitude & Units
- Correlation Coefficients & Comments
- Formulas (Inclination & Azimuth)

OWSG Prefix	Short Name	Long Name
1 A001Mc	MWD+SRGM	OWSG MWD + SRGM
3 A002Mc	MWD+SRGM+SAG	OWSG MWD + SRGM + Sag Correction
5 A003Mc	MWD+SRGM+AX	OWSG MWD + SRGM + Axial Correction
7 A004Mc	MWD+SRGM+AX+SAG	OWSG MWD + SRGM + Axial Correction + Sag Correction
9 A005Mc	MWD+IFR1	OWSG MWD + IFR1
11 A006Mc	MWD+IFR1+AX	OWSG MWD + IFR1 + Axial Corr
13 A007Mc	MWD+IFR1+AX+SAG	OWSG MWD + IFR1 + Axial Corr + Sag Correction
15 A008Mc		
17 A009Mc		
19 A010Mc		
21 A011Mc		
23 A012Mc		
25 A013Mc		
27 A014Mc		
29 A015Mc		
31 A016Mc		
33 A017Mc		
35 A018Mb		
37 A019Gb		
39 A020Gb		
41 A021Gc		
43 A022Gb		
45 A023Gb		
47 A024Mb		
49 A025Mb		
51 A026Ua		
53 A027Ub		
55 A028Ub		
57 A029Ub		
59 A030Ua		
1 B001Mc	MWD+HRGM	OWSG MWD + HRGM
3 B002Mc	MWD+HRGM+AX	OWSG MWD + HRGM + Axial Correction
5 B003Mc	MWD+HRGM+AX+SAG	OWSG MWD + HRGM + Axial Correction + Sag Correction
7 B004Mc	MWD+HRGM+SAG	OWSG MWD + HRGM + Sag Correction
9 B005Mc	MWD+HRGM+SAG+MS	OWSG MWD + HRGM + Sag + Multi-Station Correction
11 B006Mc	MWD+LRGM	OWSG MWD + LRGM
13 B007Mc	MWD+LRGM+AX	OWSG MWD + LRGM + Axial Correction
15 B008Mc	MWD+LRGM+AX+SAG	OWSG MWD + LRGM + Axial Correction + Sag Correction
17 B009Mc	MWD+LRGM+SAG	OWSG MWD + LRGM + Sag Correction
19 B010Mc	EMS+IFR1+AX+SAG	OWSG EMS + IFR1 + Axial Corr + Sag Correction
21 B011Mc	EMS+IFR1+SAG	OWSG EMS + IFR1 + Sag Correction
23 B012Mc	EMS+IFR1+AX+MS	OWSG EMS + IFR1 + Sag + Multi-Station Correction
25 B013Mc	EMS+HRGM	OWSG EMS + HRGM
27 B014Mc	EMS+HRGM+AX	OWSG EMS + HRGM + Axial Correction
29 B015Mc	EMS+HRGM+AX+SAG	OWSG EMS + HRGM + Axial Correction + Sag Correction
31 B016Mc	EMS+HRGM+SAG	OWSG EMS + HRGM + Sag Correction
33 B017Mc	EMS+LRGM	OWSG EMS + LRGM
35 B018Md	EMS+LRGM+AX	OWSG EMS + LRGM + Axial Correction
37 B019Md	EMS+LRGM+AX+SAG	OWSG EMS + LRGM + Axial Correction + Sag Correction
39 B020Mc	EMS+LRGM+SAG	OWSG EMS + LRGM + Sag Correction
41 B021Ga	FINDS	OWSG BHI Ferranti FINDS
42 B022Ua	BLIND+TREND	OWSG BLIND+TREND

Set B
Extended

<https://www.iscwsa.net/error-model-documentation/>

Example: A001Mc MWD+SRGM

https://www.iscwsa.net/error-code-model-documentation/ISCWSA_Generic_Toolcodes_SetA_Rev5-1 (updated 23/9/22)
Excel Workbook Tab: MWD+SRGM

Header Reference Information

ABBMc: MWD-SRGM

OU/SG Prefix: ABBMc

Short Name: MWD-SRGM

Long Name: OWSG MWD + SRGM

Revision No: 5.3

Revision Date: 8-Oct-20

Revision Comment: [Detailed revision notes including changes to match ISCWSA Model Rev 5, XCLB & XCLH terms, and various tool code updates.]

Application: MWD using 1 Year Standard Resolution Geomagnetism Mode (e.g. BDOG up to 2018, MWSD) with no additional corrections

Tool Type: Magnetometer

Status: []

Checked: []

Approved: []

Notes: Based on ISCWSA MWD Rev 3 (Tool Face Independent - Sliding)

Revision History: Rev 5.1 05-Jun-2010 Draft Release for Comment

Indication Range Min: 0 deg

Indication Range Max: 180 deg

Hor East/Vest Evolution: 0 deg

Flange Comment: None

Tool Parameters: Misalignment Alt: 3

Misalignment Min Course Length: 10 m

WCL_Torsionity: 1 deg/1000 ft

No	Code	Term Description	Vt.Fn.	Vt.Fn. Source	Type	Magnitude	Units	Prop.	P1	P2	P3	Vt.Fn. Comment	Depth	Form	Inclination	Formula	Azimuth Formula
11	CRFR	Depth, Depth Reference - Random	CRFR	SPE 6796	Depth	0.25	m	R	0	0	0		1	0			0
12	DSFS	Depth, Depth Scale Factor - Systematic	DSFS	SPE 6796	Depth	0.0005	-	S	1	0	0		MD	0			0
9	DSTG	Depth, Depth Stretch - Global	DST	SPE 6796	Depth	0.00000205	1/m	G	1	1	1		MD * TVD	0			0
4	ABXY-TI	MWD TF Ind. X and Y Accelerometer Bias	ABXY-TI	SPE 63275 - Andy Broo	Sensor	0.004	m/s ²	S	1	0	0		0	-Cos(Inc) / Gfield		(Tan(Dip) * Cos(Inc) * Sin(AzM)) / Gfield	
5	ABXY-TZ	MWD TF Ind. X and Y Accelerometer Bias	ABXY-TZ	SPE 63275 - Andy Broo	Sensor	0.004	m/s ²	S	1	0	0		0	0		(Tan(Dip) * Sin(Inc) * Cos(AzM)) / Gfield	
6	ABZ	MWD-Z-Accelerometer Bias	ABZ	SPE 6796 Table 1	Sensor	0.004	m/s ²	S	1	0	0		0	-Sin(Inc) / Gfield		Tan(Dip) * Sin(Inc) * Sin(AzM) / Gfield	
7	ASXY-TI	MWD TF Ind. X and Y Accelerometer Bias	ASXY-TI	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0		0	Sin(Inc) * Cos(Inc) / Sqr2		(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / Sqr2	
8	ASXY-TZ	MWD TF Ind. X and Y Accelerometer Bias	ASXY-TZ	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0		0	0		(Tan(Dip) * Sin(Inc) * Sin(AzM)) / 2	
9	ASXY-TI	MWD TF Ind. X and Y Accelerometer Bias	ASXY-TI	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0		0	0		(Tan(Dip) * Sin(Inc) * Sin(AzM) * Cos(Inc)) / 2	
10	ASZ	MWD-Z-Accelerometer Bias	ASZ	SPE 6796 Table 1	Sensor	0.004	m/s ²	S	1	0	0		0	0		0	(Sin(Inc) * Sin(AzM)) / (BFW4 * Cos(Dip))
11	MBXY-TI	MWD TF Ind. X and Y Magnetometer Bias	MBXY-TI	SPE 63275 - Andy Broo	Sensor	70	nT	S	1	0	0		0	0		0	Cos(Inc) * Sin(AzM) / (BFW4 * Cos(Dip))
12	MBXY-TZ	MWD TF Ind. X and Y Magnetometer Bias	MBXY-TZ	SPE 63275 - Andy Broo	Sensor	70	nT	S	1	0	0		0	0		0	Cos(Inc) * Sin(AzM) * Cos(Dip)
13	MBZ	MWD-Z-Magnetometer Bias	MBZ	SPE 6796 Table 1	Sensor	70	nT	S	1	0	0		0	0		0	-Sin(Inc) * Sin(AzM) / (BFW4 * Cos(Dip))
14	MSXY-TI	MWD TF Ind. X and Y Magnetometer Scale Factor	MSXY-TI	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0		0	0		0	Sin(Inc) * Sin(AzM) * (Tan(Dip) * Cos(Inc) * Sin(AzM)) / (BFW4 * Cos(Dip))
15	MSXY-TZ	MWD TF Ind. X and Y Magnetometer Scale Factor	MSXY-TZ	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0		0	0		0	Sin(Inc) * Sin(AzM) * (Tan(Dip) * Sin(Inc) * Cos(Inc)) / (BFW4 * Cos(Dip))
16	MSZ	MWD-Z-Magnetometer Scale Factor	MSZ	SPE 6796 Table 1	Sensor	0.0005	-	S	1	0	0		0	0		0	Sin(Inc) * Sin(AzM) * (Tan(Dip) * Sin(Inc) * Sin(AzM)) / (BFW4 * Cos(Dip))
17	MSZ	MWD-Z-Magnetometer Scale Factor	MSZ	SPE 6796 Table 1	Sensor	0.0005	-	S	1	0	0		0	0		0	Sin(Inc) * Sin(AzM) * (Tan(Dip) * Sin(Inc) * Sin(AzM) * Cos(Inc)) / (BFW4 * Cos(Dip))
18	DEC	MWD Declination Crustal Omission Error	DEC	SPE 6796 Table 1	AsPiel	0.05	deg	G	1	1	1		0	0		0	1
19	DEC-OS	MWD Declination Crustal Omission Error	DEC-OS	SPE 6796 Table 1	AsPiel	0.05	deg	G	1	1	1		0	0		0	1
20	DEC-OH	MWD Declination Crustal Omission HD Models	DEC-OH	SPE 6796 Table 1	AsPiel	0.21	deg	G	1	1	1		0	0		0	1
21	DEC-OI	MWD Declination Crustal Omission IFR Models	DEC-OI	SPE 6796 Table 1	AsPiel	0.05	deg	G	1	1	1		0	0		0	1
22	DEC-R	MWD Declination - Random	DEC-R	SPE 6796 Table 1	AsPiel	0.1	deg	R	0	0	0		0	0		0	1
23	DEH-U	MWD BH Dependent Declination Uncorrelated Errors	DEH-U	SPE 6796 Table 1	AsPiel	0.2	deg	R	0	0	0		0	0		0	1/ (BFW4 * Cos(Dip))
24	DEH-S	MWD BH Dependent Declination Crustal Omission Standard	DEH-S	SPE 6796 Table 1	AsPiel	0.2	deg	R	0	0	0		0	0		0	1/ (BFW4 * Cos(Dip))
25	DEH-OH	MWD BH Dependent Declination Crustal Omission HD Models	DEH-OH	SPE 6796 Table 1	AsPiel	0.2	deg	R	0	0	0		0	0		0	1/ (BFW4 * Cos(Dip))
26	DEH-OI	MWD BH Dependent Declination Crustal Omission IFR Models	DEH-OI	SPE 6796 Table 1	AsPiel	0.2	deg	R	0	0	0		0	0		0	1/ (BFW4 * Cos(Dip))
27	DEH-R	MWD BH Dependent Declination - Random	DEH-R	SPE 6796 Table 1	AsPiel	3000	deg/nT	R	0	0	0		0	0		0	1/ (BFW4 * Cos(Dip))
28	AML	MWD Azial Interference - Slat Sin A	AML	Hubertson	Magnet	220	nT	S	1	0	0		0	0		0	Sin(Inc) * Sin(AzM) / (BFW4 * Cos(Dip))
29	SAGE	MWD Sag	SAGE	ISCWSA	Align	0.2	deg	S	1	0	0		0	0		0	(Sin(Inc)) ^{0.25}
30	XYM1	Misalignment: XY Misalignment 1	XYM1	SPE 90408 Table 9 - AR	Align	0.1	deg	S	1	0	0		0	0		0	Abs(Sin(Inc))
31	XYM2	Misalignment: XY Misalignment 2	XYM2	SPE 90408 Table 9 - AR	Align	0.1	deg	S	1	0	0		0	0		0	-1
32	XYME	Misalignment: XY Misalignment 3	XYME	ISCWSA	Align	0.3	deg	R	0	0	0		0	0		0	Cos(Inc) * Cos(AzT) * Max(L, sqrt(10*(MD-MDP))) * (Cos(Inc) * Sin(AzT) / Sin(Inc)) * Max(L, sqrt(10*(MD-MDP)))
33	XYME	Misalignment: XY Misalignment 4	XYME	ISCWSA	Align	0.3	deg	R	0	0	0		0	0		0	Cos(Inc) * Sin(AzT) * Max(L, sqrt(10*(MD-MDP))) * (Cos(Inc) * Cos(AzT) / Sin(Inc)) * Max(L, sqrt(10*(MD-MDP)))
34	XCLA	Depth, Long Course Length XCL - Azimuth	XCLA	SPE 97249 Jerry Codlin	Depth	6.97	-	R	0	0	0		0	0		0	Max(Sin(Abs(AzT-AdPiel)), WCLTorsionity * (MD-MDP)) / S
35	XCLH	Depth, Long Course Length XCL - Inclination	XCLH	SPE 97249 Jerry Codlin	Depth	6.97	-	R	0	0	0		0	0		0	Max(Sin(Abs(AzT-AdPiel)), WCLTorsionity * (MD-MDP)) / S

MWD PUM Survey Corrections

Axial (AX)

Sag

Multi-Station Analysis (MSA or MS)

Axial + Sag

Multi-Station + Sag

Depth Corrections

Advanced MWD Corrections

Ground Shot (GS) IFR

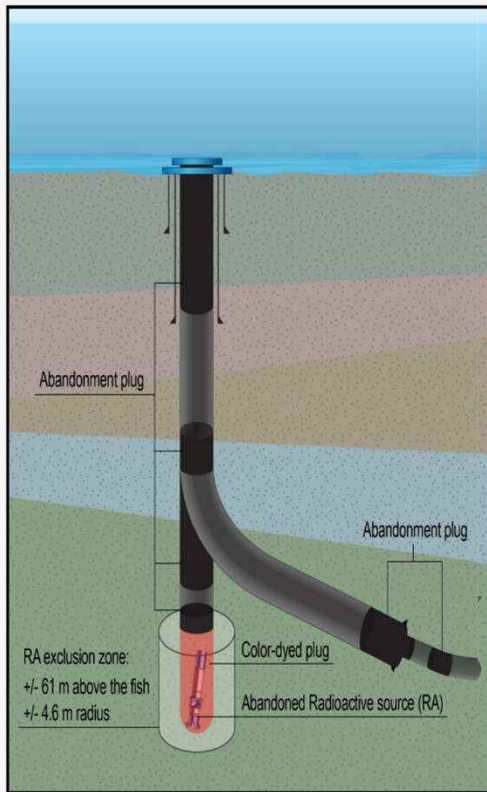
Advanced Multi-Station (AMSA)

All BHA's for a Wellbore

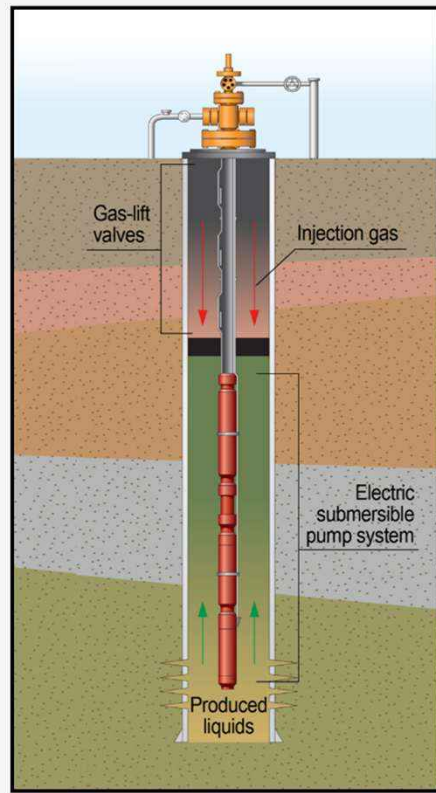
All BHA's for all wellbores on a well (Includes Sidetracks / By-Pass Wellbores)

All BHA's for all wellbores on a Site/Location/Pad

Offset Well Environment



MASD Management Principles (SPE-187073-PA)



Offset Well Environment

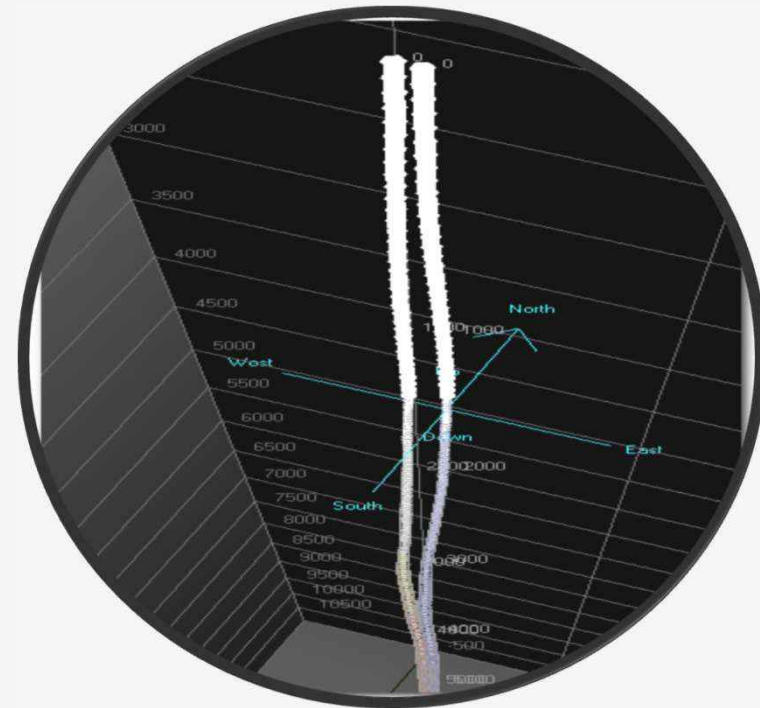
- Status
- Completion Type
- Wellbore Fluids
- Lifting Mechanism

Artificial Lift

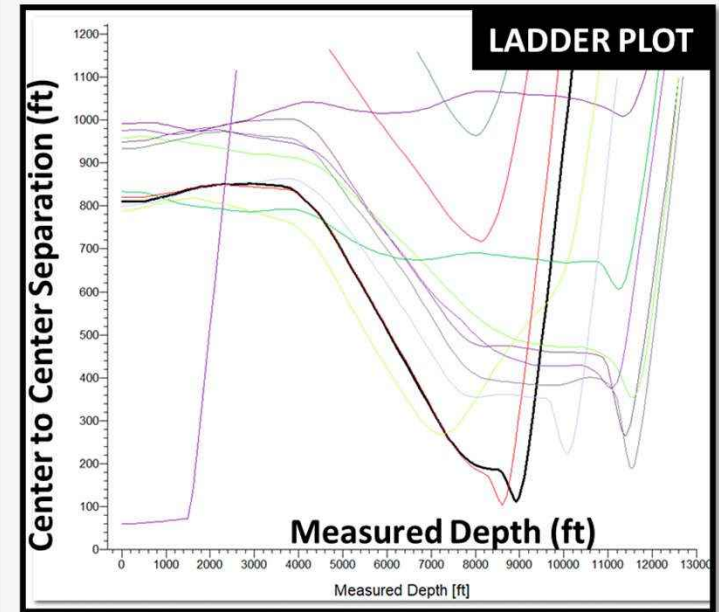
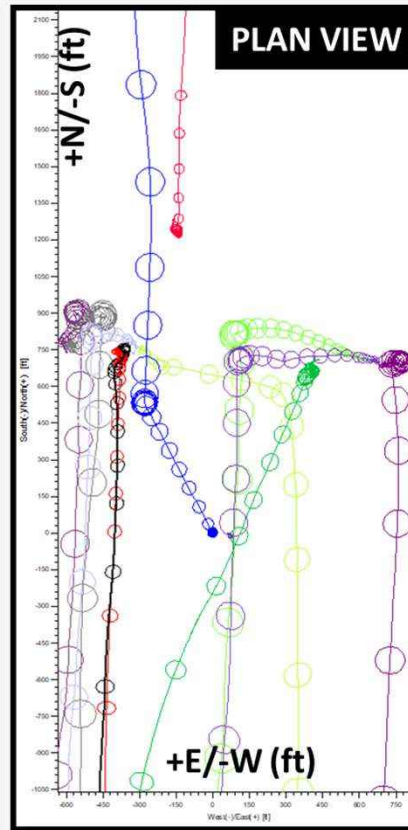
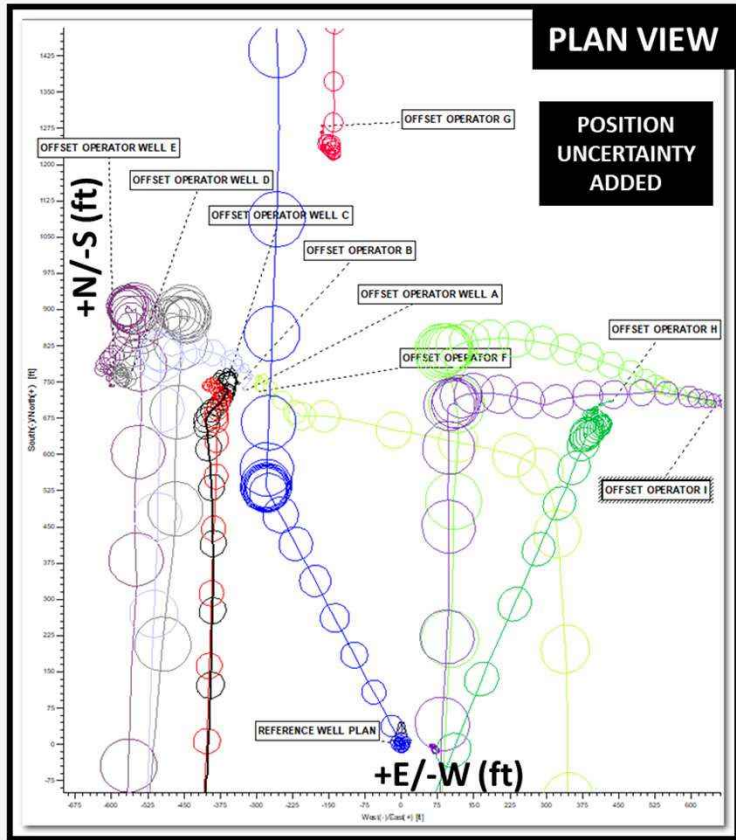
- Rod Pump
- Progressive Cavity
- Hydraulic Pump
- Gas Lift (GL)
- Electric Submersible Pump (ESP)
- Hybrid Lift System
 - GL & ESP
 - ESP & Natural Flow

Case Study

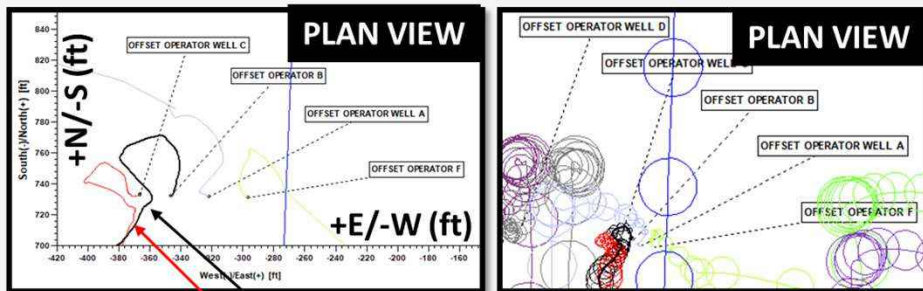
Offset Operator Close Approach



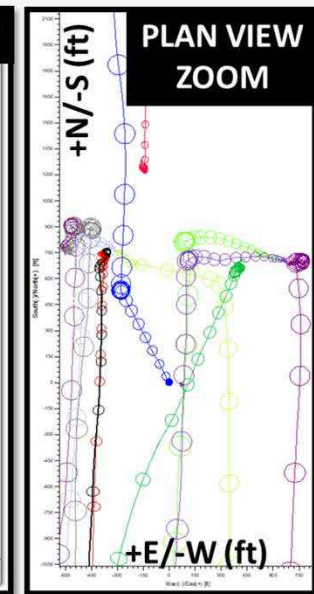
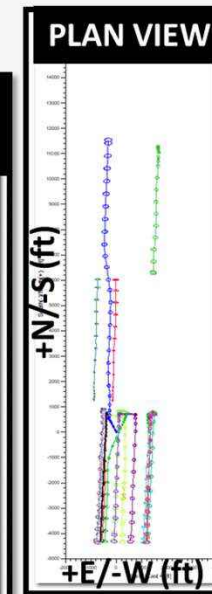
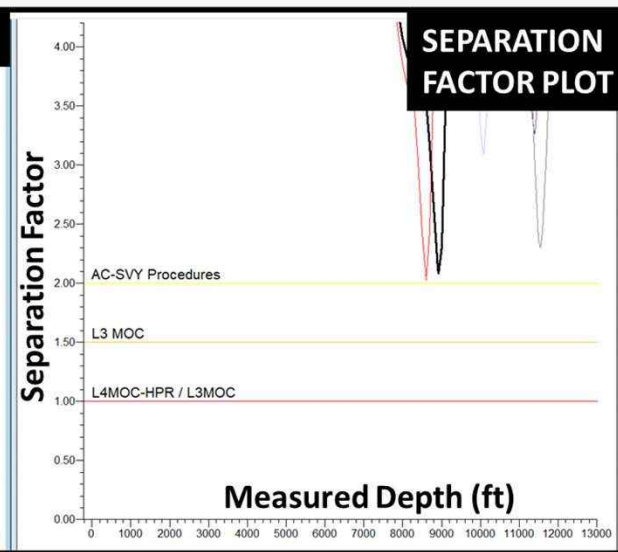
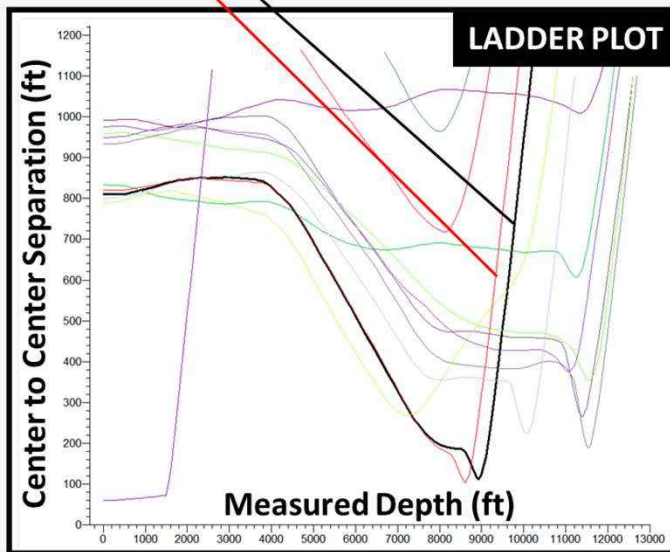
Safe Separation Plots – Ladder & Separation Factor



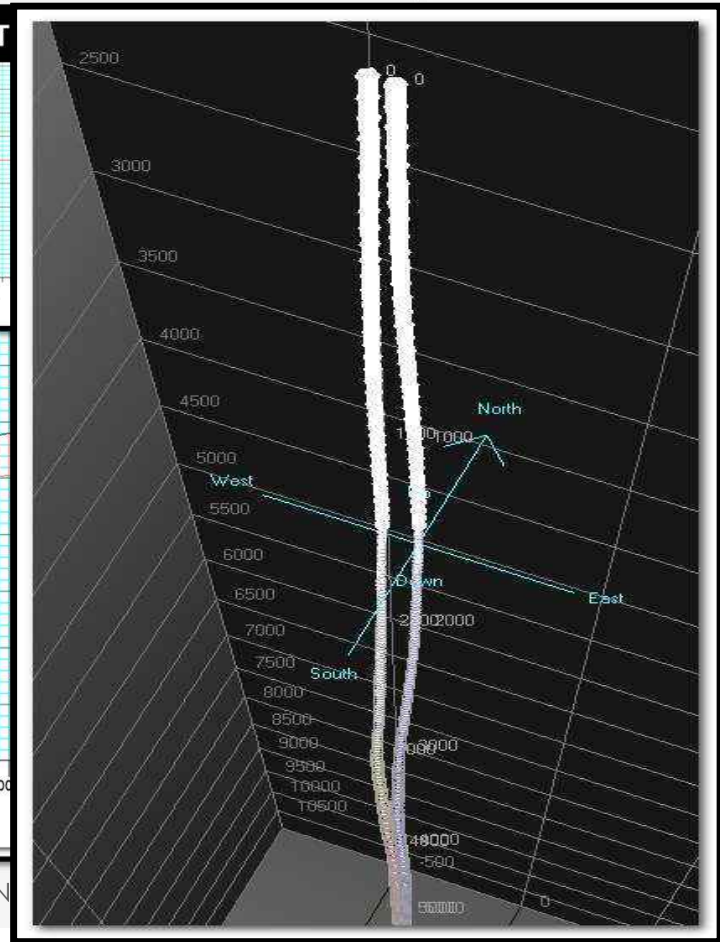
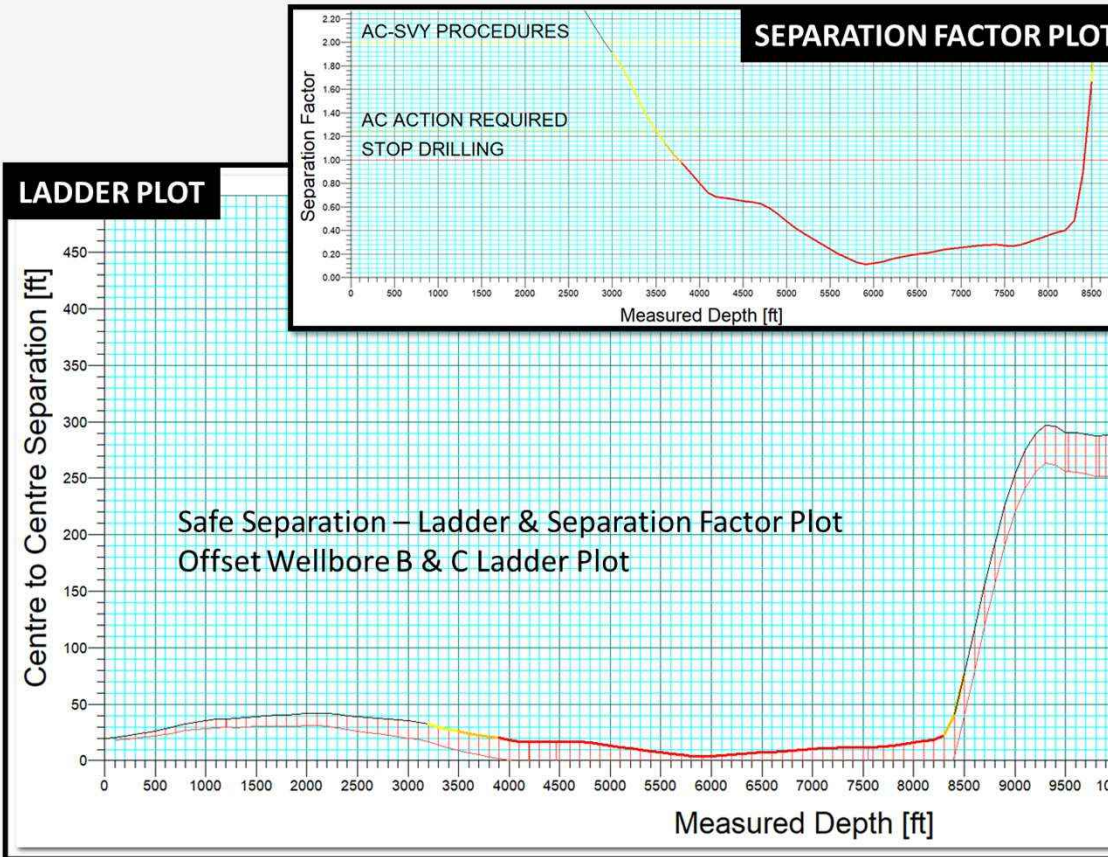
Safe Separation Plots – Ladder & Separation Factor



Offset B & C Indicates similar distance from planned well (Blue) which means these wellbore are very close from each other. They are neighboring slots on a four well pad drilled by another Operator.



Safe Separation Plots – Ladder & Separation Factor



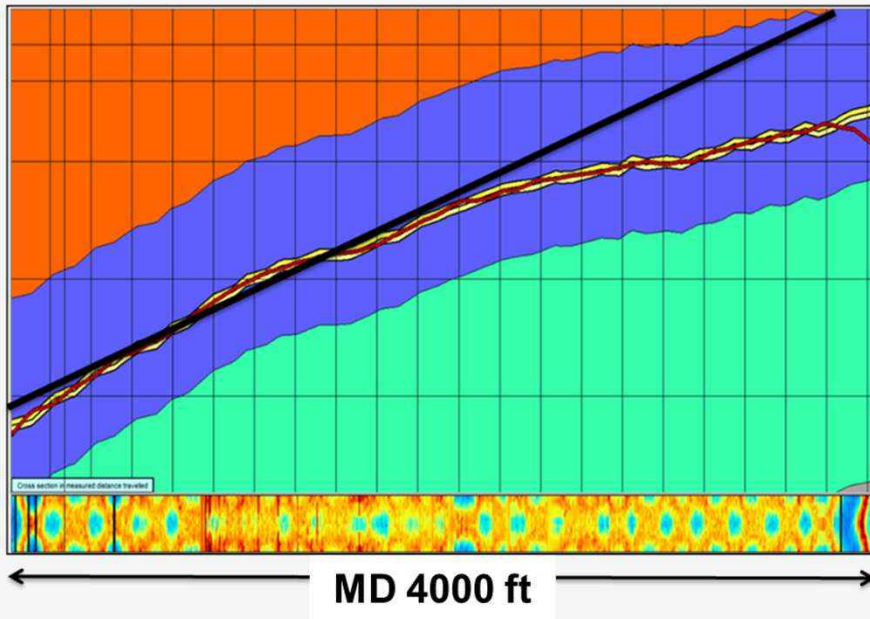
Case Study



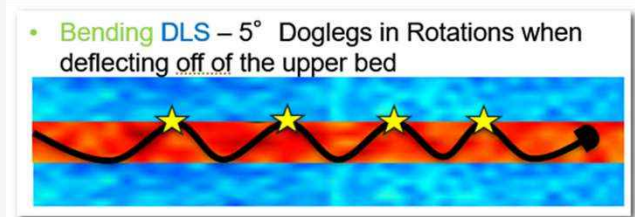
Lateral Undulations
Key Performance Indicators
Steerable Motor Curve
Lateral Tortuosity



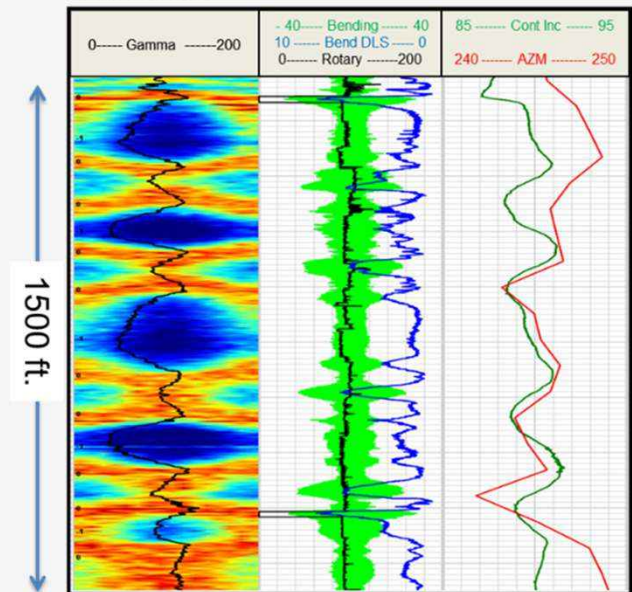
Lateral Undulation Period - TVD Accuracy



- What if the well plan diverges from the 'locked in' bed?
- If not identified then the DD may make a correction to go back to plan



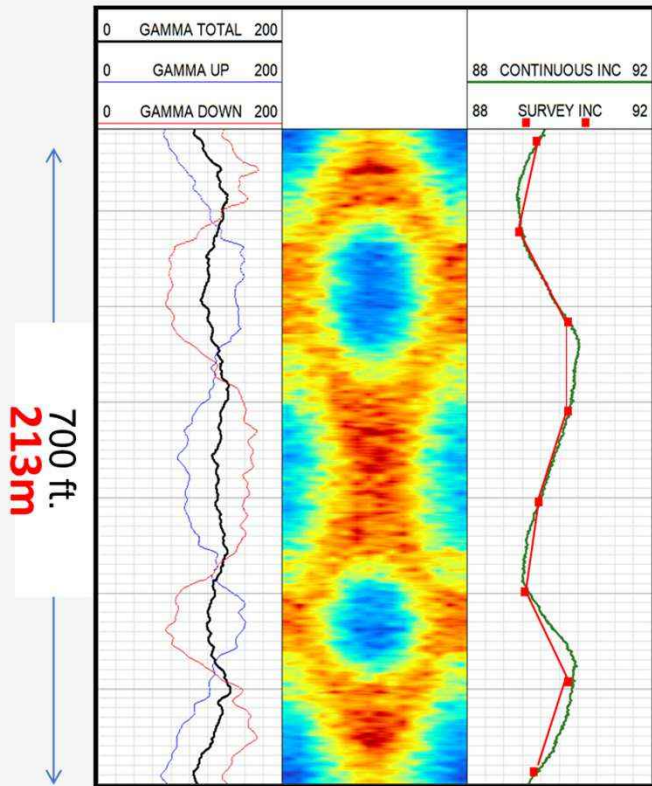
Pad 3 Well A



Viens, Christopher , Clark, Tyler , Lightfoot, Jonathan , and Carlos Mercado. "Real-Time Downhole Data Resolves Lithology Related Drilling Behavior." Paper presented at the IADC/SPE Drilling Conference and Exhibition, Fort Worth, Texas, USA, March 2018. doi: <https://doi.org/10.2118/189697-MS>

Lateral Undulation Period - TVD Accuracy

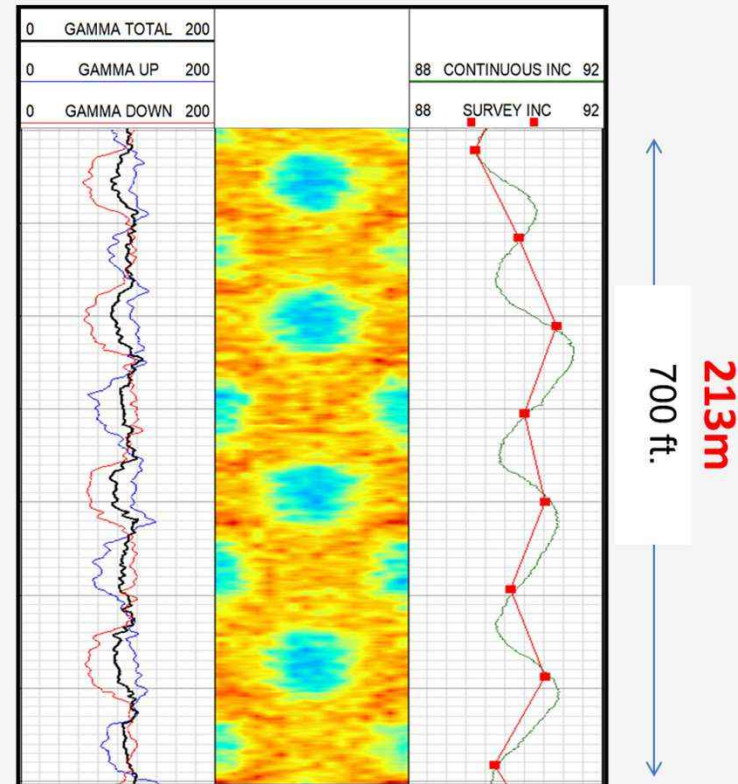
Pad 2 Well A



Left: 90' (27m) surveys adequate to due large period of oscillation

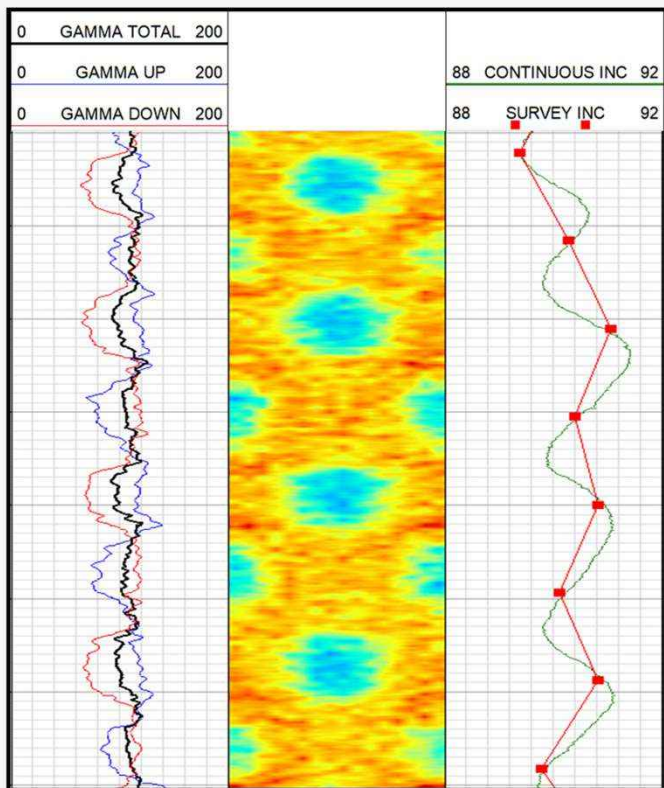
Right: 90'(27m) surveys inadequate to short oscillation period

Pad 1 Well A



Lateral Undulation Period - TVD Accuracy

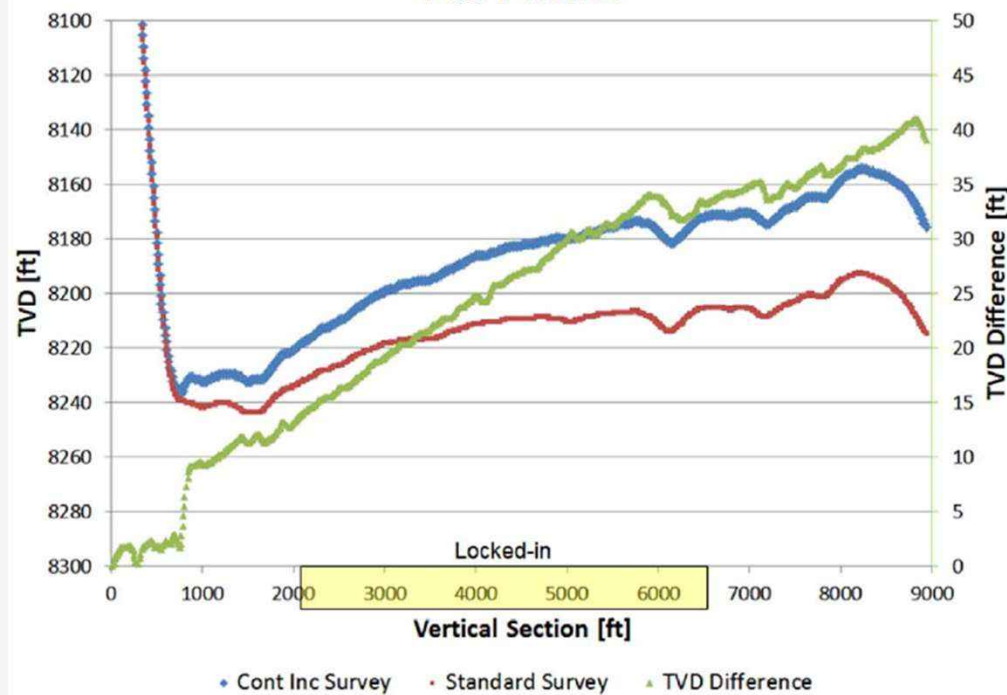
Pad 1 Well A



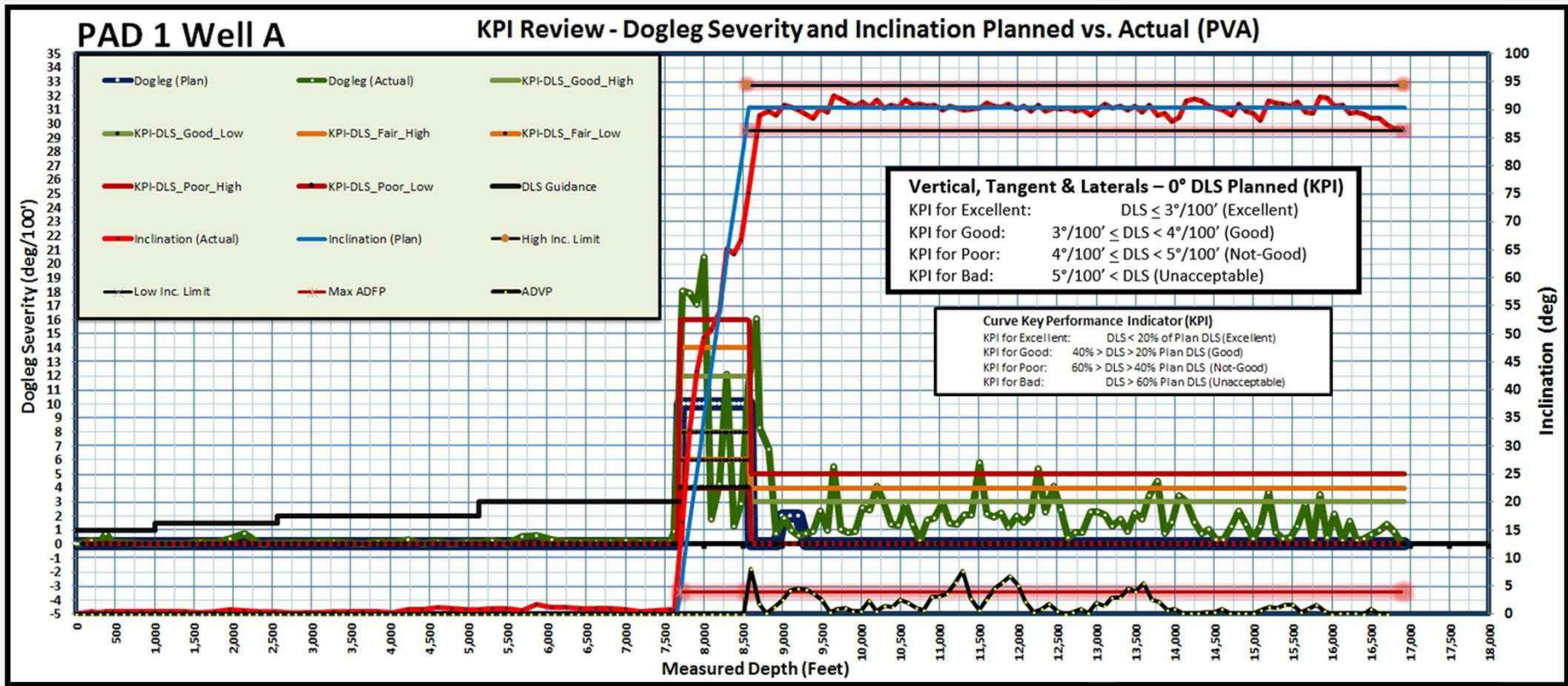
213m
700 ft.

40ft (12.2m) Delta in TVD at the end of the lateral

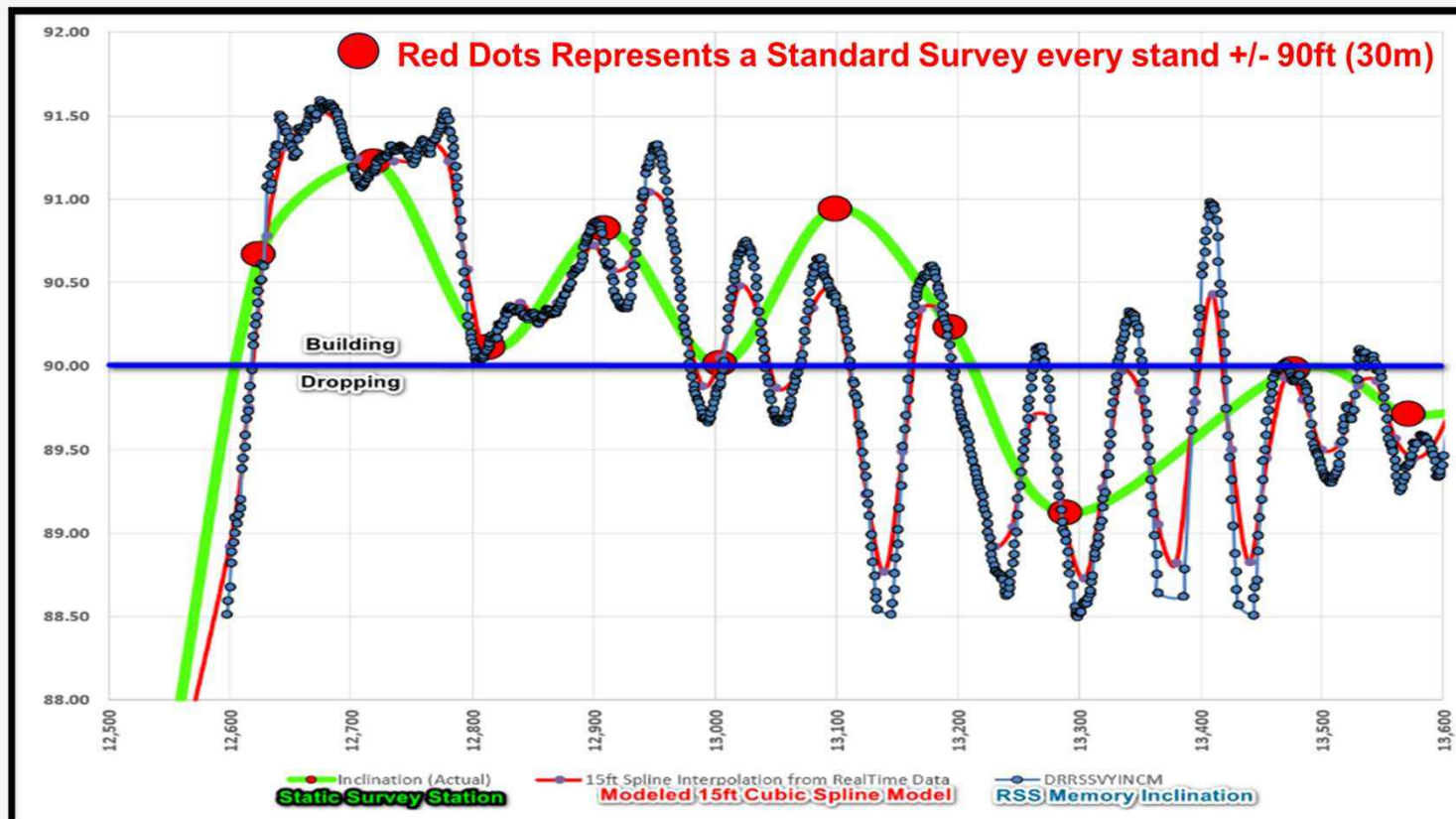
Pad 1 Well A



Directional Drilling Key Performance Indicators



Lateral Undulation Period – RSS Example



Slide / Rotate Effect – Curve TVD Accuracy

Starting Survey = 10,000 ft (3048m) MD

Inclination 30° (9m) & Azimuth 45°

- Case A: Slide 30 ft (9m) then Rotate 70 ft (21m) @ 10°/100'
- Case B: Rotate 70 ft (21m) then Slide 30 ft (9m) @ 10°/100' (30m)

Final Inclination 40° & Final Azimuth 45°

Case A: Survey at 10,030' & at 10,100'

- DLS 16.7°/100 ft & TVD 9,082.6 ft (2768.4m)

Case B: Survey at 10,070' & at 10,100'

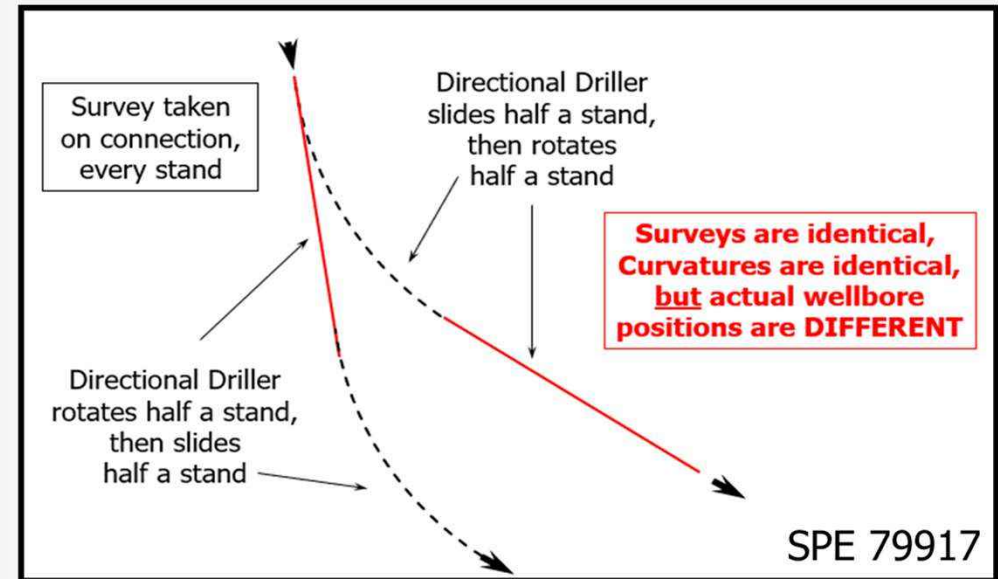
- DLS 16.67°/100 ft & TVD 9,085.9 ft (2769.4m)

Case C: Survey only at 10,100'

- DLS 5°/100 ft & TVD 9,084 ft (2768.8m)

Case A vs. Case B have a TVD difference 3.29 ft (1m) over only 100 ft of MD (1-Stand)

A total of 29.6 ft of TVD Difference between Case A and Case B

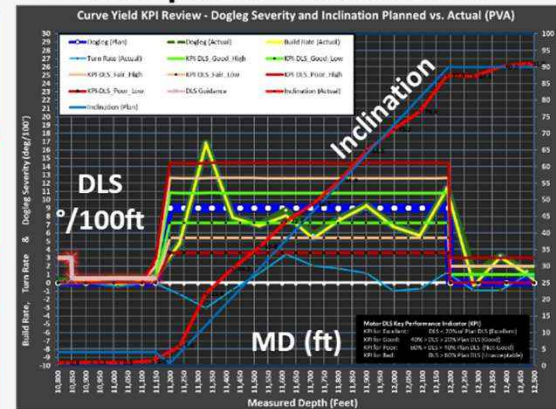


Consider the full curve build up section from Vertical to Horizontal @ 10°/100 ft (30m). This difference represents 900 ft ((274m) MD which equals 29.6 ft (9m) of TVD Difference in the Landing Depth

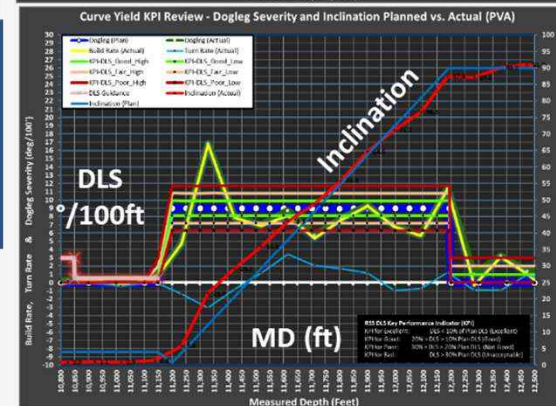
Directional Drilling Key Performance Indicators

Directional Drilling Dogleg Severity Control Key Performance Indicators				
Directional Tools & Hole Section Type	Excellent	Good	Not-Good	Unacceptable RCRA Required
Vertical Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Tangent Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Lateral Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Directional Motor Steering Interval	DLS < +/- 20% of Planned DLS	Between 20-40% of Planned DLS	Between 40-60% of Planned DLS	DLS > +/- 60% of Planned DLS
Directional RSS Steering Interval	DLS < +/- 10% of Planned DLS	Between 10-20% of Planned DLS	Between 20-30% of Planned DLS	DLS < +/- 30% of Planned DLS

Offset Operator Motor Curve



**Motor Curve
KPI Chart
20-40-60%**



**RSS Curve
KPI Chart
10-20-30%**

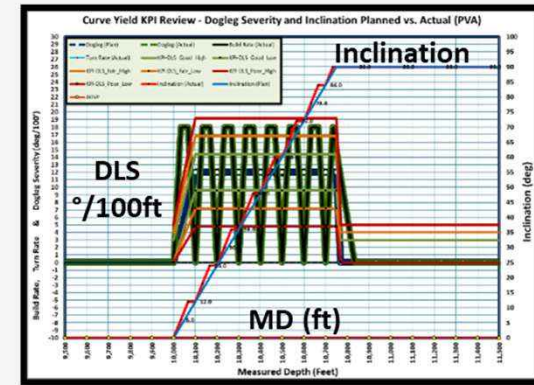
Slide / Rotate Effect – Curve TVD Accuracy

Case A: Slide 33 ft, Rotate 33 ft and Slide 33 ft from 0° to 90° Inc.

MD	Inclination (Actual)	Azimuth (Actual)	Course Length	TVD	Vertical Section	+N / -S	+E / -W	Colours Distance	@ AZM	Dogleg (Actual)	Build Rate (Actual)	Turn Rate (Actual)
0.00	0.00	45.00	*****	0.00	0.00	0.00	0.00	0.00	45.00	0.00	*****	*****
10,000.00	0.00	45.00	10000.00	10000.00	0.00	0.00	0.00	0.00	45.00	0.00	0.00	0.00
10,033.33	6.00	45.00	33.33	10033.27	1.26	1.23	1.23	1.75	45.00	18.00	18.00	0.00
10,066.67	12.00	45.00	33.33	10066.18	3.03	4.92	4.92	6.96	45.00	18.00	18.00	0.00
10,100.00	18.00	45.00	33.33	10099.78	10.05	9.82	9.82	13.89	45.00	0.00	0.00	0.00
10,133.33	24.00	45.00	33.33	10130.97	16.29	15.92	15.92	22.51	45.00	18.00	18.00	0.00
10,166.67	30.00	45.00	33.33	10162.07	24.92	24.36	24.36	34.45	45.00	18.00	18.00	0.00
10,200.00	36.00	45.00	33.33	10192.52	34.73	33.95	33.95	48.01	45.00	0.00	0.00	0.00
10,233.33	42.00	45.00	33.33	10222.11	45.67	44.64	44.64	63.13	45.00	18.00	18.00	0.00
10,266.67	48.00	45.00	33.33	10250.55	58.89	57.47	57.47	79.82	45.00	18.00	18.00	0.00
10,300.00	54.00	45.00	33.33	10277.78	74.47	72.71	72.71	98.07	45.00	0.00	0.00	0.00
10,333.33	60.00	45.00	33.33	10303.87	92.60	90.51	90.51	117.84	45.00	18.00	18.00	0.00
10,366.67	66.00	45.00	33.33	10328.87	113.27	110.93	110.93	139.09	45.00	0.00	0.00	0.00
10,400.00	72.00	45.00	33.33	10352.87	136.58	133.93	133.93	161.80	45.00	18.00	18.00	0.00
10,433.33	78.00	45.00	33.33	10375.94	162.64	159.64	159.64	196.06	45.00	18.00	18.00	0.00
10,466.67	84.00	45.00	33.33	10398.09	191.46	187.46	187.46	242.01	45.00	18.00	18.00	0.00
10,500.00	90.00	45.00	33.33	10419.36	223.03	218.03	218.03	299.56	45.00	0.00	0.00	0.00
10,533.33	96.00	45.00	33.33	10439.78	257.34	251.34	251.34	369.49	45.00	18.00	18.00	0.00
10,566.67	102.00	45.00	33.33	10459.36	294.39	287.39	287.39	451.70	45.00	0.00	0.00	0.00
10,600.00	108.00	45.00	33.33	10478.09	334.18	326.18	326.18	547.19	45.00	18.00	18.00	0.00
10,633.33	114.00	45.00	33.33	10495.94	376.65	367.65	367.65	656.84	45.00	0.00	0.00	0.00
10,666.67	120.00	45.00	33.33	10512.94	421.78	411.78	411.78	780.63	45.00	18.00	18.00	0.00
10,700.00	126.00	45.00	33.33	10529.11	469.57	458.57	458.57	919.56	45.00	0.00	0.00	0.00
10,733.33	132.00	45.00	33.33	10544.48	519.99	507.99	507.99	1074.63	45.00	18.00	18.00	0.00

Case A Directional Survey

SIMULATED EXAMPLE

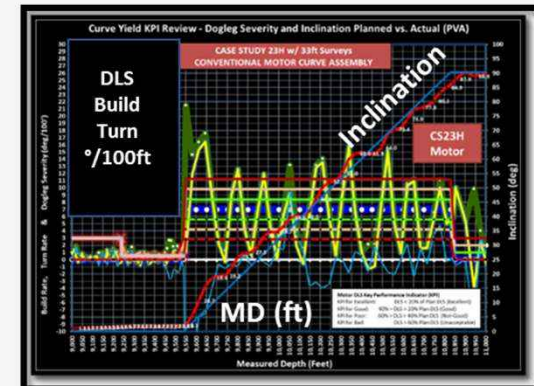


Case B: Survey Every 100 ft from 0° to 90° Inc. (16 ft TVD Delta)

MD (Plan)	Inclination (Plan)	Azimuth (Plan)	Course Length	TVD	Vertical Section	+N / -S	+E / -W	Closure	@ AZM	Dogleg (Plan)	Build Rate	Turn Rate
0.00	0.00	0.00	*****	0.00	0.00	0.00	0.00	0.00	0.00	0.00	*****	*****
10,000.00	0.00	45.00	10000.00	10000.00	0.00	0.00	0.00	0.00	45.00	0.00	0.00	0.45
10,100.00	12.00	45.00	100.00	10092.57	7.55	7.8	7.8	1.43	45.00	12.00	12.00	0.00
10,200.00	24.00	45.00	100.00	10184.50	29.10	29.1	29.1	4.28	45.00	12.00	12.00	0.00
10,300.00	36.00	45.00	100.00	10275.00	65.48	64.8	64.8	9.19	45.00	12.00	12.00	0.00
10,400.00	48.00	45.00	100.00	10364.83	114.29	111.71	111.71	15.98	45.00	12.00	12.00	0.00
10,500.00	60.00	45.00	100.00	10453.50	172.71	168.81	168.81	238.73	45.00	12.00	12.00	0.00
10,600.00	72.00	45.00	100.00	10541.10	238.68	233.29	233.29	329.92	45.00	12.00	12.00	0.00
10,700.00	84.00	45.00	100.00	10474.85	309.32	302.33	302.33	427.56	45.00	12.00	12.00	0.00
10,750.00	90.00	45.00	50.00	10477.48	345.42	337.62	337.62	477.46	45.00	12.00	12.00	0.00

Case B Directional Survey

ACTUAL EXAMPLE

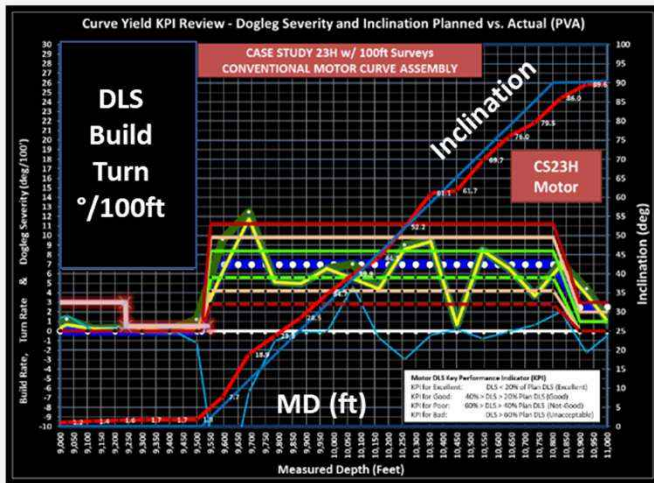


Case Study - Steerable Motor Curve

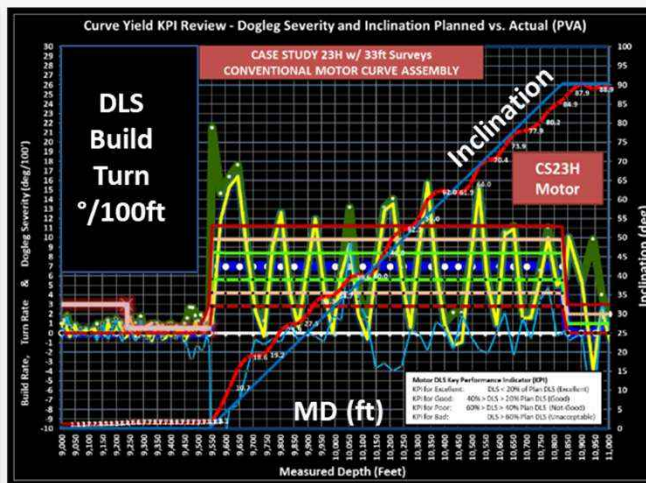
- Survey Frequency is Important for Medium Radius Curves (Build Section)
- If slide % is less, consider surveying twice a stand or every joint
- When sliding > 75 ft (27m) per Stand survey position is less prone to TVD error

Takeaway: Use a Smaller Bent Housing and Slide more footage in the Curve!

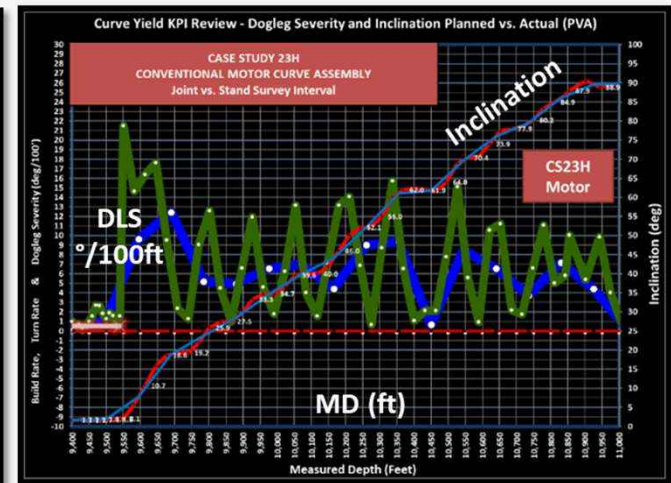
96 FT SURVEYS



32 FT SURVEYS



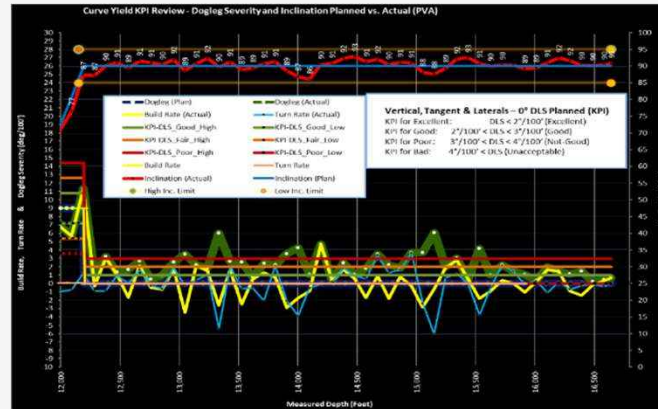
DLS COMPARISON



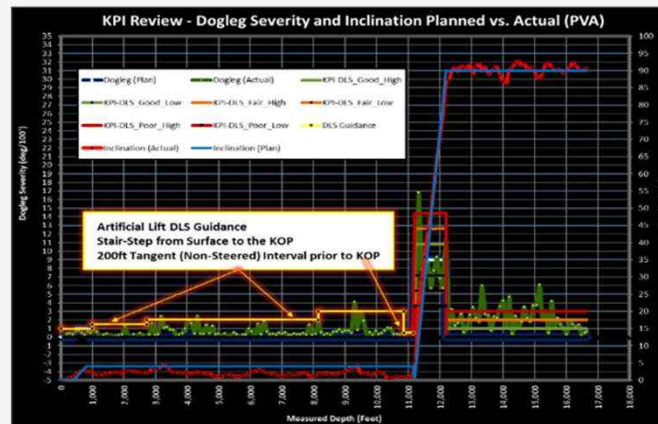
Lateral Tortuosity KPI – Case Study

Establish KPI's based on expected maximum dogleg severity

- Surface
- Tangent
- Curve
- Lateral



Lateral DLS Build & Turn Rate KPI Chart With Inclination +/- Allowable Deviation from Plan

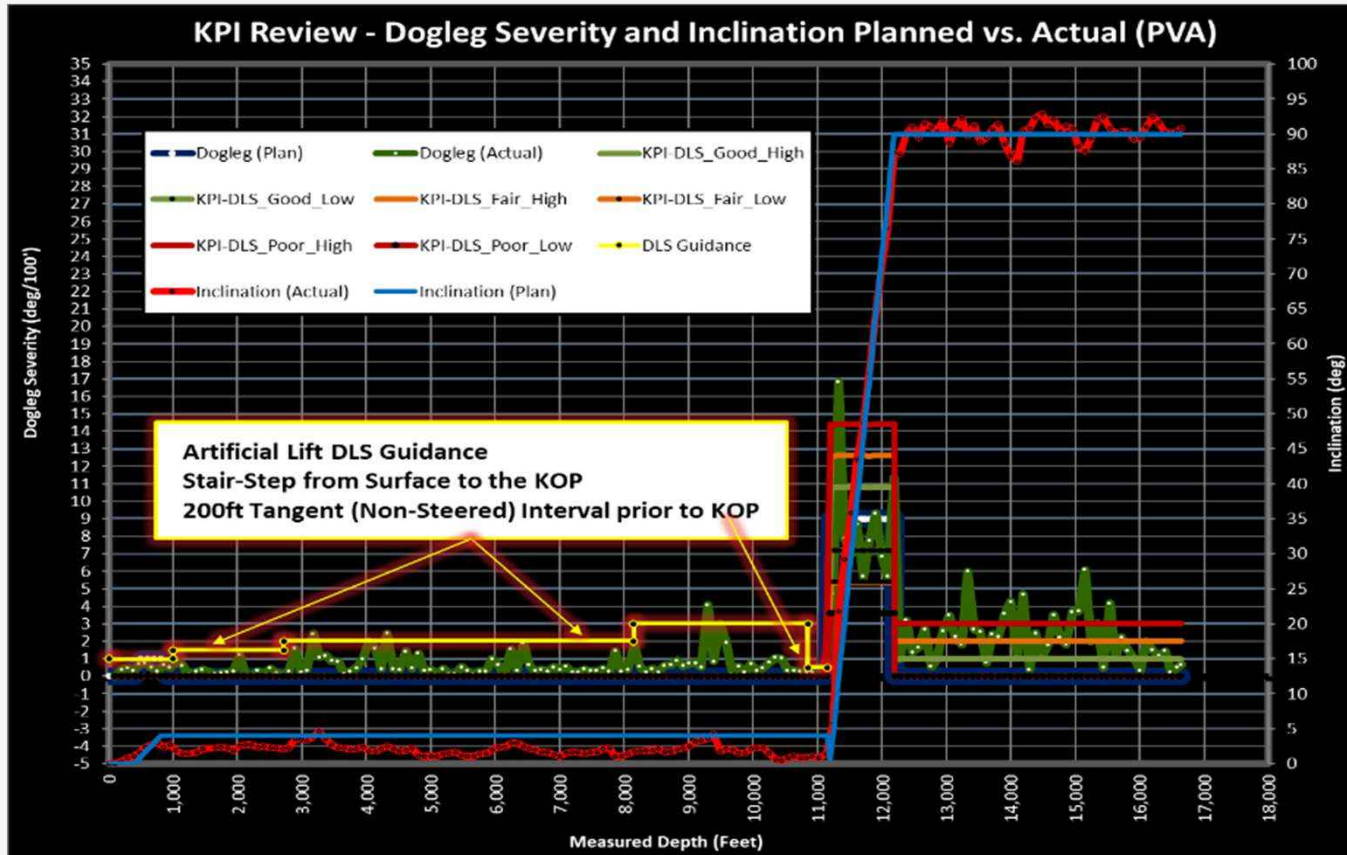


Surface to TD DLS KPI Chart with Artificial Lift DLS Guidance for Surface & Intermediate

Directional Drilling Dogleg Severity Control Key Performance Indicators

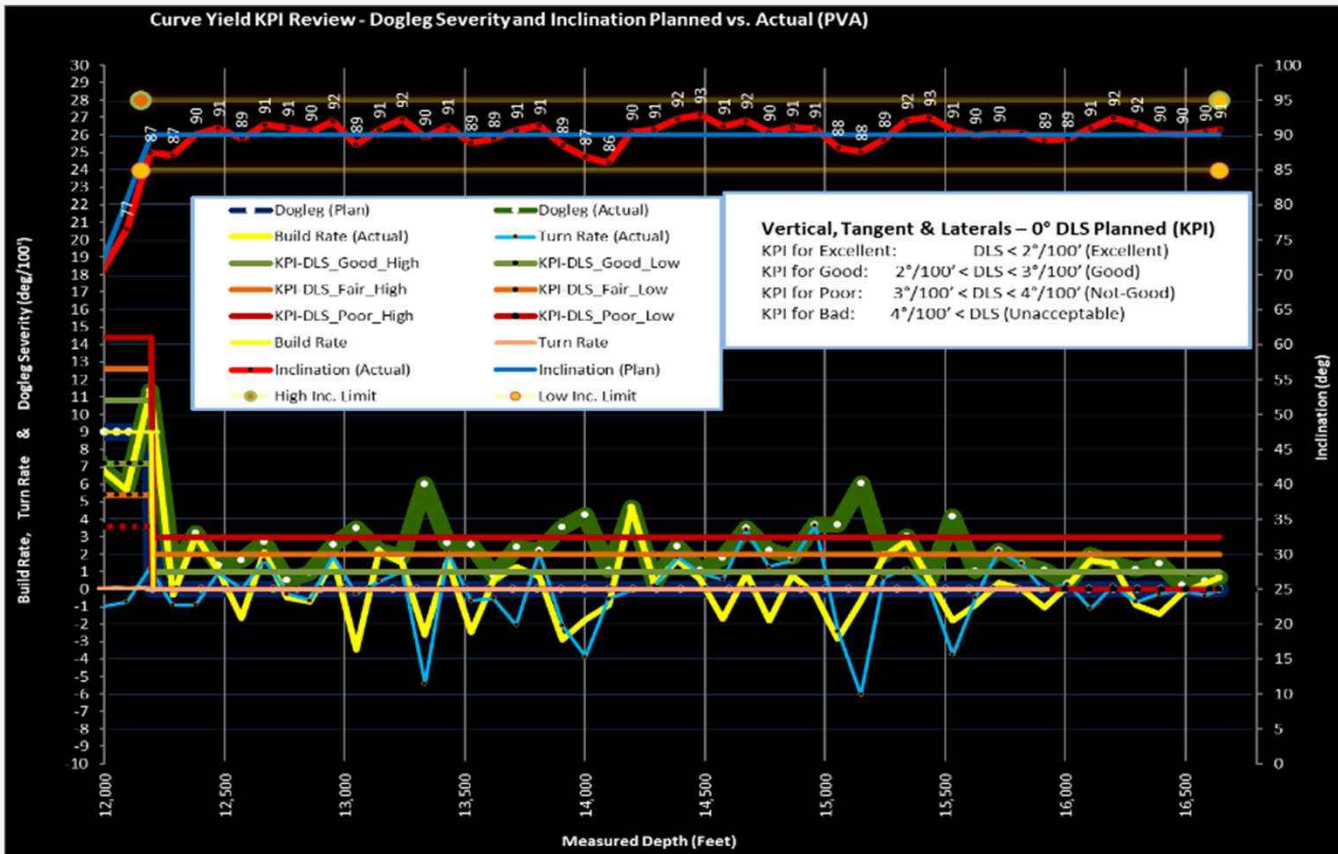
Directional Tools & Hole Section Type	Excellent	Good	Not-Good	Unacceptable RCRA Required
Vertical Intervals	DLS ≤ 2	2 < DLS ≤ 3	3 < DLS ≤ 4	4 < DLS
Tangent Intervals	DLS ≤ 2	2 < DLS ≤ 3	3 < DLS ≤ 4	4 < DLS
Lateral Intervals	DLS ≤ 2	2 < DLS ≤ 3	3 < DLS ≤ 4	4 < DLS
Directional Motor Steering Interval	DLS < +/- 20% of Planned DLS	Between 20-40% of Planned DLS	Between 40-60% of Planned DLS	DLS > +/- 60% of Planned DLS
Directional RSS Steering Interval	DLS < +/- 10% of Planned DLS	Between 10-20% of Planned DLS	Between 20-30% of Planned DLS	DLS < +/- 30% of Planned DLS

Lateral Tortuosity KPI – Case Study



Surface
to TD DLS
KPI Chart with
Artificial Lift DLS
Guidance for
Surface &
Intermediate

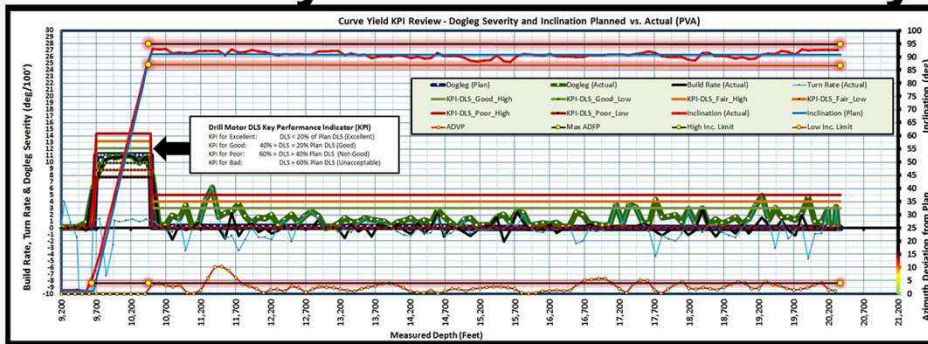
Lateral Tortuosity KPI – Case Study



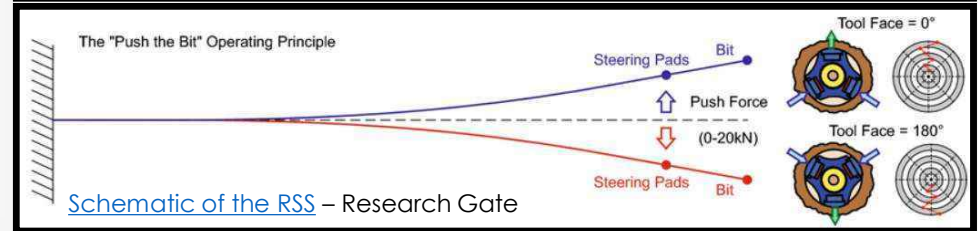
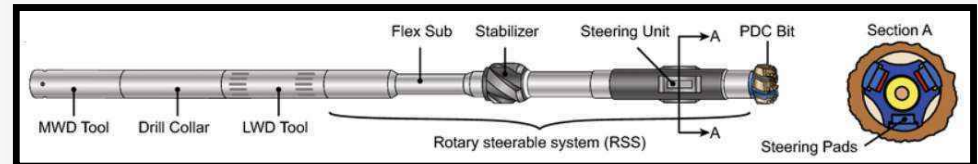
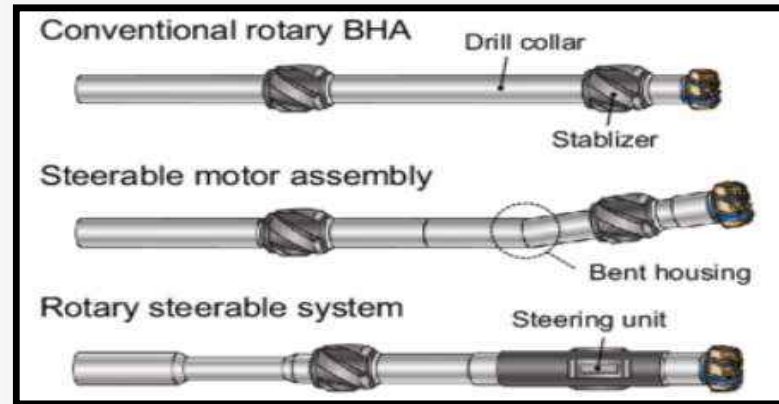
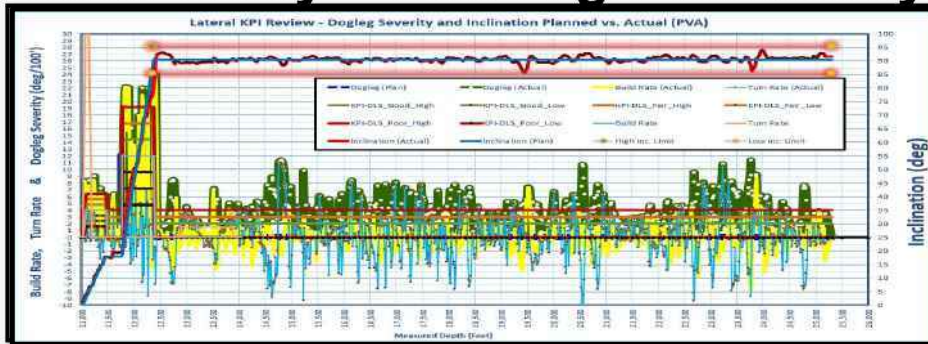
Lateral DLS
 Build & Turn
 Rate KPI Chart
 With Inclination
 +/- Allowable
 Deviation from
 Plan

Curve Lateral Tortuosity KPI - RSS Examples

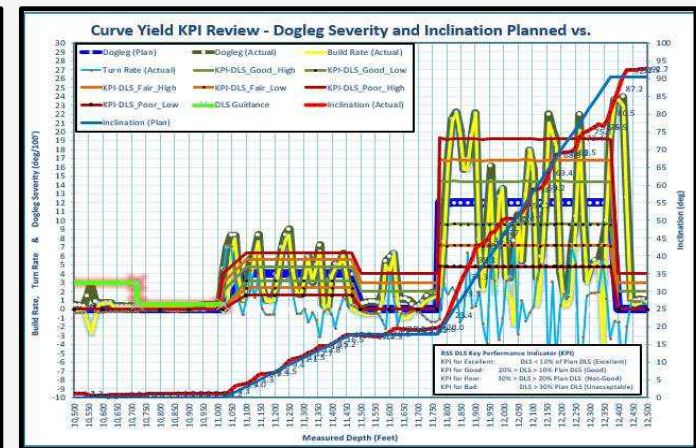
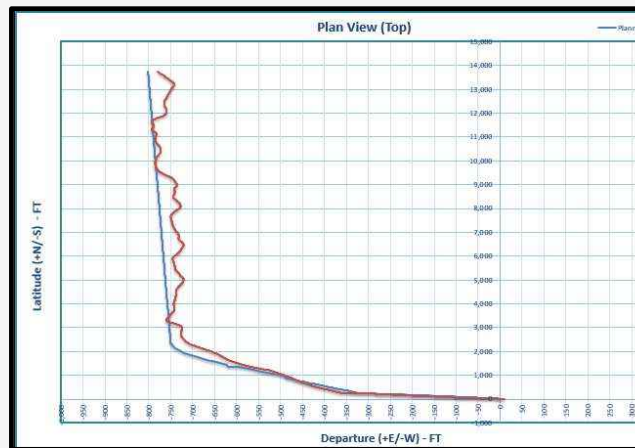
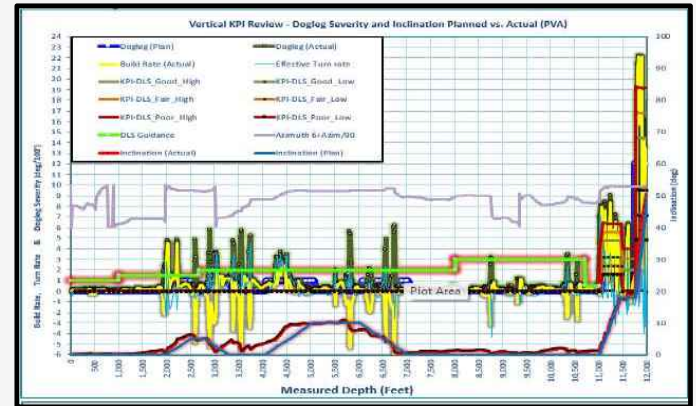
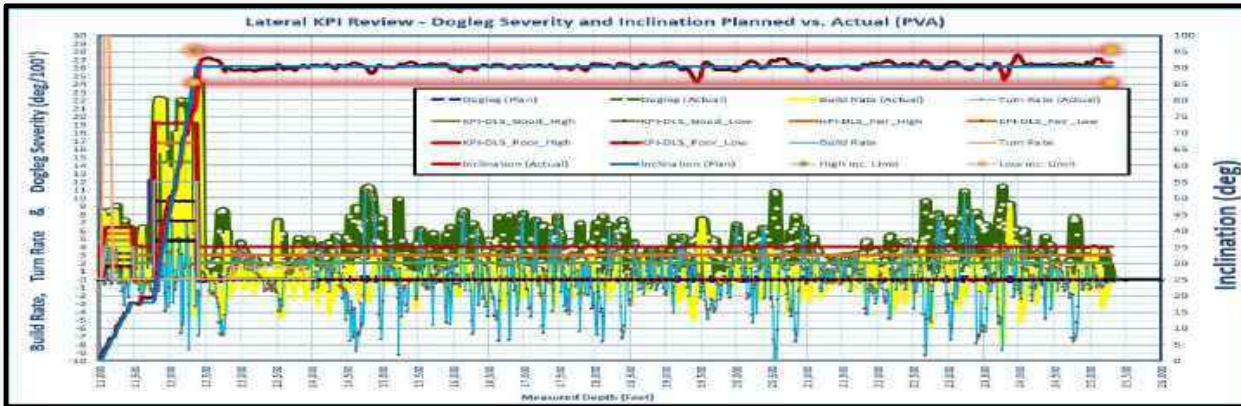
Case Study – RSS Low Tortuosity



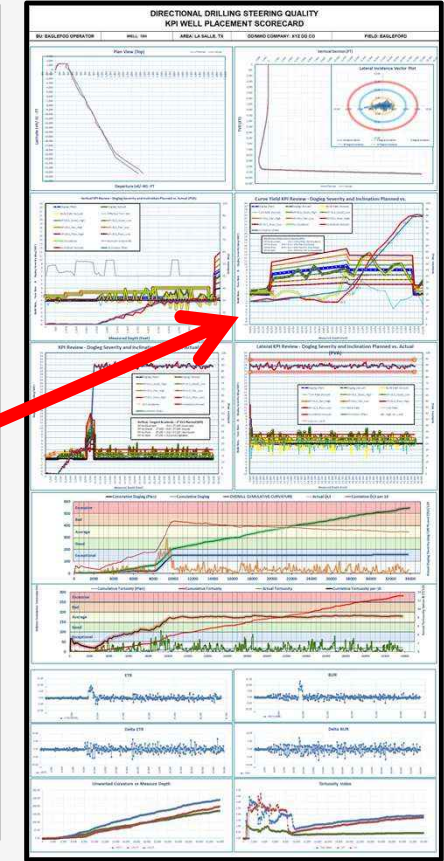
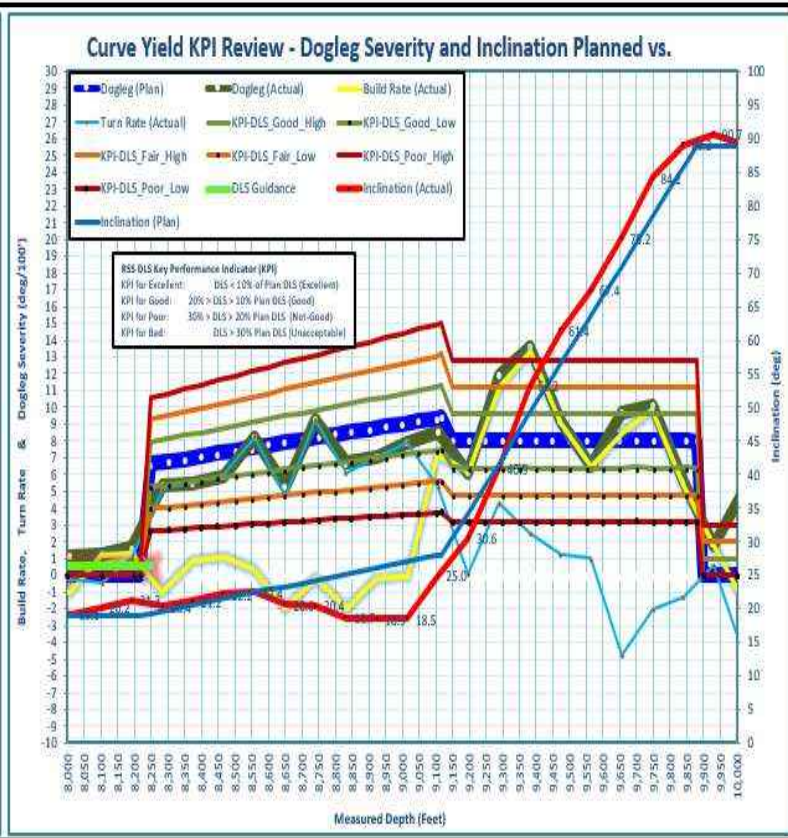
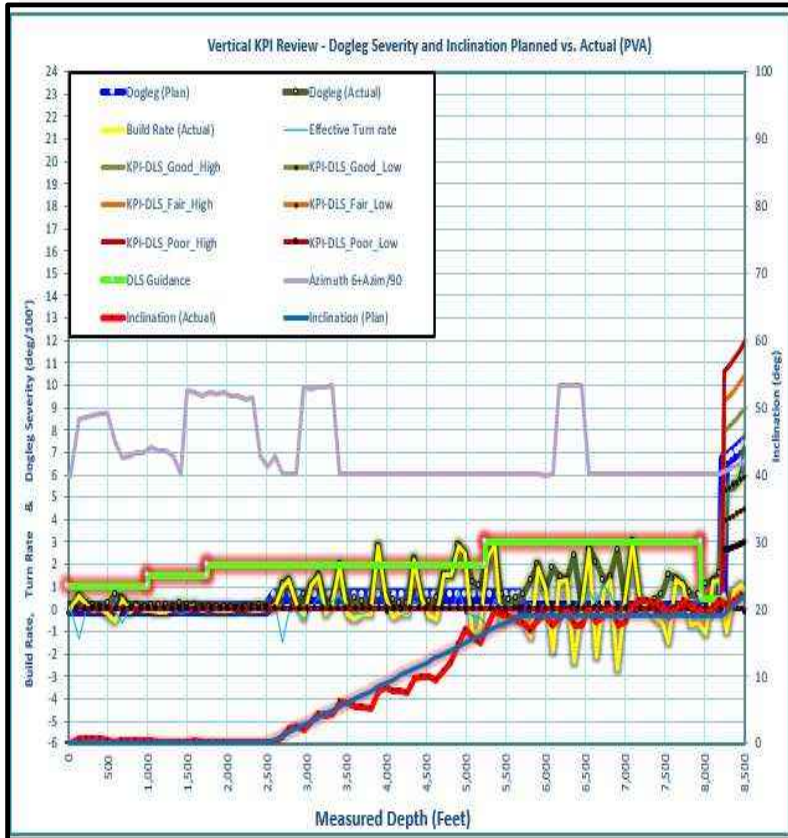
Case Study – RSS High Tortuosity



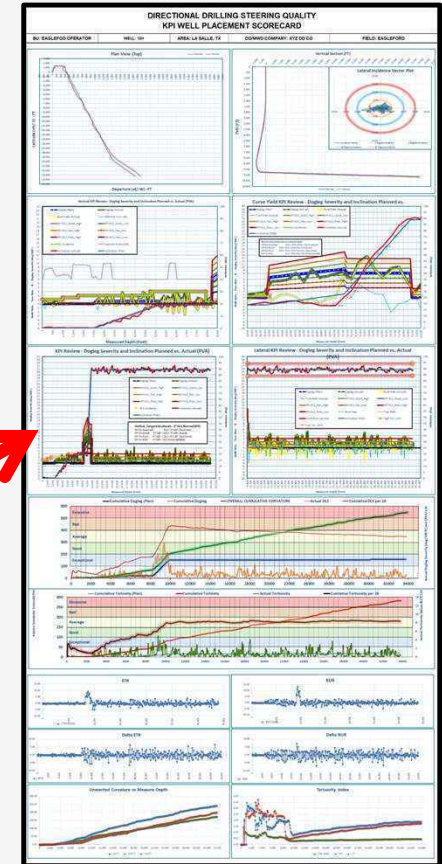
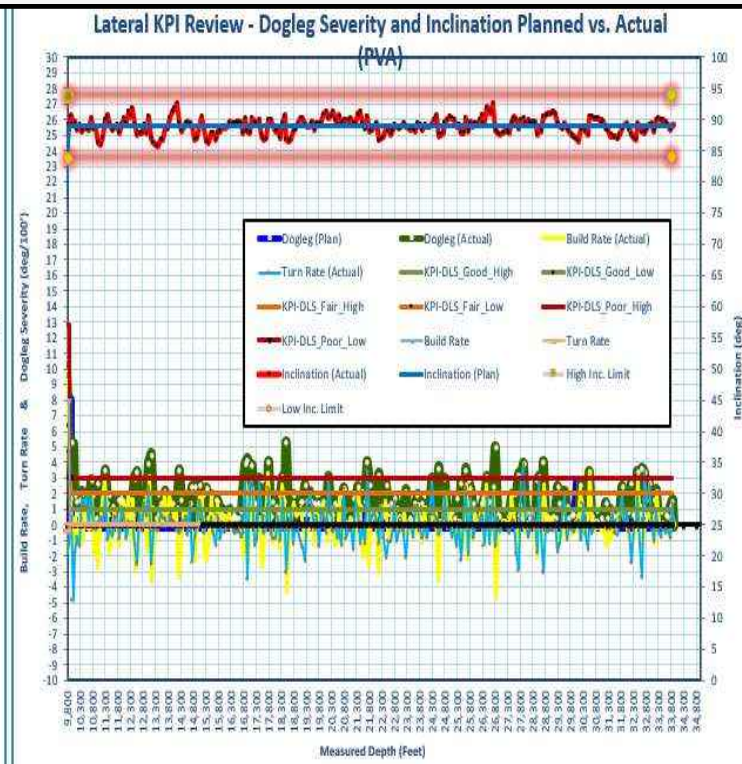
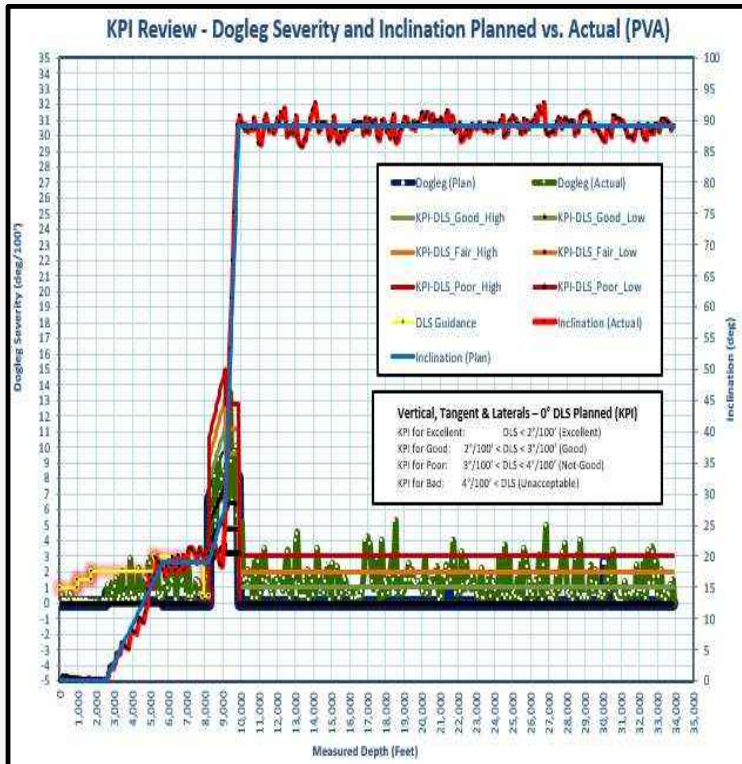
Curve Lateral Tortuosity KPI - RSS Example



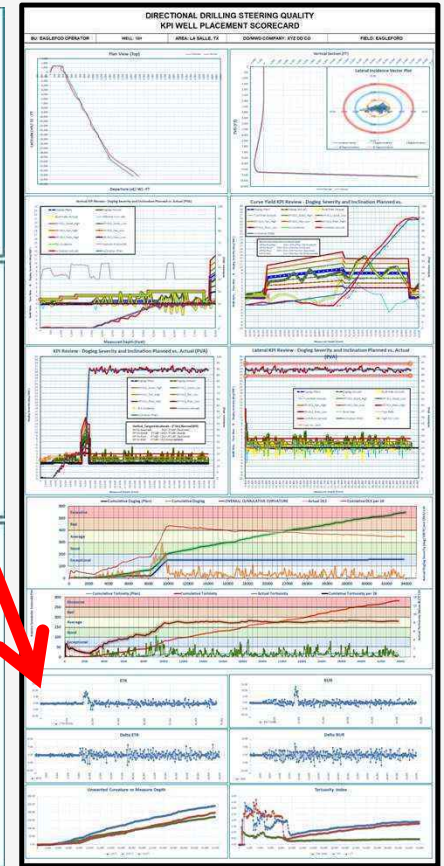
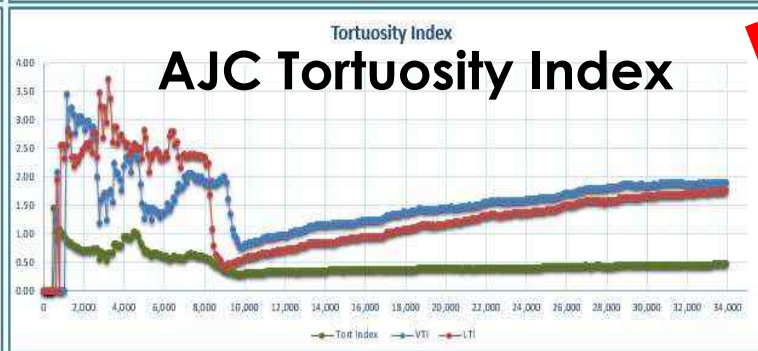
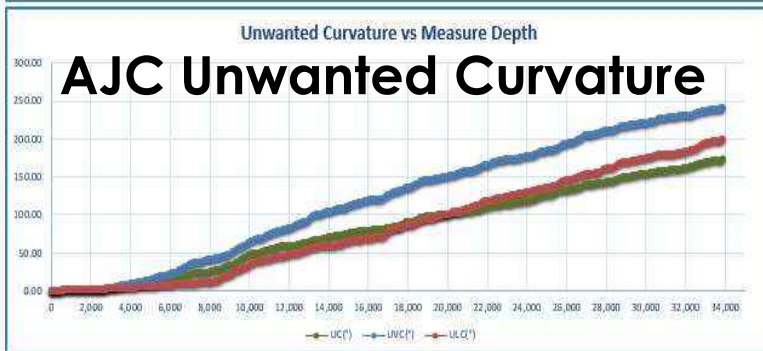
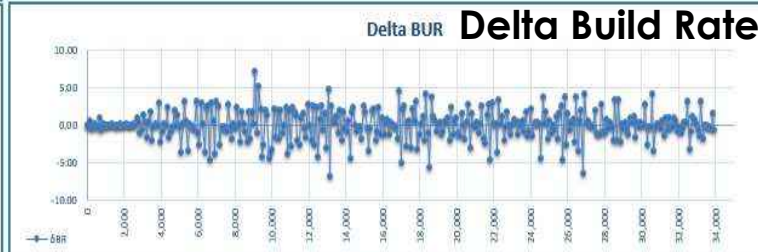
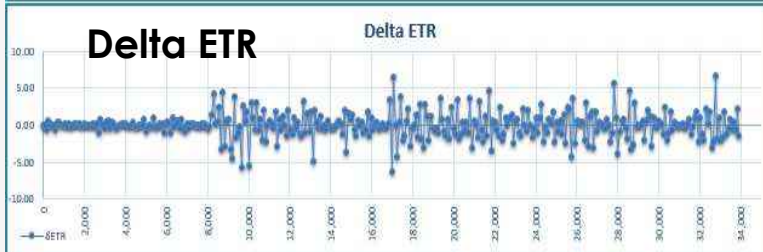
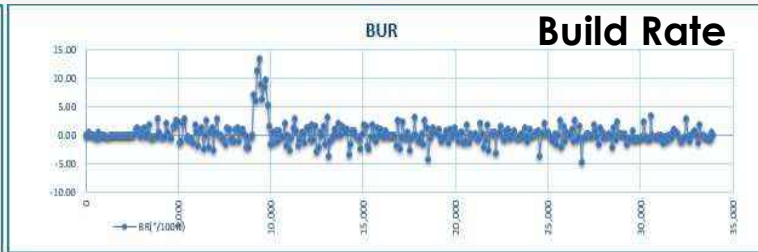
TX EXAMPLE – DirDrIlg KPI SCORECARD



TX EXAMPLE – DirDrIlg KPI SCORECARD



TX EXAMPLE – DirDrlg KPI SCORECARD



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Key Takeaways



- As demonstrated in these case studies, Safe Separation collision avoidance methods are designed to safely separate wellbores while also improving wellbore position accuracy.
- The survey interval should be considered during both the drilling planning and execution phases.
- Key performance indicators aid in achieving the objectives and expectations of directional wells.
- Wellbore Surveying and Positioning Practices
 - Provides a primary source of technical information for all subsurface borehole construction applications.
 - Contributes to the modernization of the wellbore construction industry by promoting safe separation procedures.
 - All participants in wellbore construction should support the collaborative effort of a committed group of industry volunteers. The desired outcome is industry-wide adoption.



API RP78 Status Update

How far we have come...

- 2012 - OWSG Formed (Operator's Wellbore Survey Group)
- 2015 - [SPE-178843-MS OWSG Std Survey Error Model Set](#) (Published March 2016)
- 2016 - API DPOS RP 78 Task Group – 3/2/2016 & [SPE-178843-MS OWSG Std Survey Error Model Set](#)
- 2017 – SPE WPTS / ISCWSA QA/QC Text Reduction for Magnetic-Gyro-Depth
- 2018 – [SPE Well-Collision-Avoidance Management and Principles SPE-184730-PA](#)
- 2019 – BSEE Report on Surveying & [SPE Well-Collision-Avoidance Separation Rule PA Paper SPE-187073-PA](#)
- 2020 – Combined 1st Build of Document
- 2021 – API Working Draft
- 2022 – Recommended Practice Technical Writing & Editing
- 2023 - AADE National Technical Conference & Exhibition (NTCE) Paper
 - [Introduction to API RP 78, Wellbore Surveying and Positioning](#) (Lightfoot/Tank-Oxy & Coco-API)
- 2023 – Pre-Ballot Revision
- 2024 – Final Ballot Preparation & Technical Edits
- 2025 – Balloting & Consensus
- 2025–26 Ballot Comment Resolution – (In Progress)

AADE AADE-23-NTCE-073



INTRODUCTION TO API RP78

Jonathan Lightfoot (Oxy)

Will Tank (Oxy)

Ben Coco (API)

AADE-23-NTCE-073



Introduction to API RP 78, *Wellbore Surveying and Positioning*

Jonathan D. Lightfoot and Will Tank, Oxy; Ben Coco, API

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Abstract

The American Petroleum Institute (API) recently undertook the development of a document called Recommended Practice 78, *Wellbore Surveying and Positioning*, (RP 78), a modern technical industry standard for wellbore placement that can be applied to all wellbore construction applications. The standard is intended to serve as the primary technical reference for proven engineering practices in the applications of oil and gas, geothermal, carbon sequestration, coalbed methane (CBM), horizontal directional drilling (HDD) trenchless boring, mineral ventilation and extraction, scientific coring, and all other subsurface borehole construction applications.

API RP 78's development was led by a group of independent consultants, industry experts, academics, and representatives from public and private energy operators. The Operator's Wellbore Survey Group (OWSG), which later became an official sub-committee of the Industry Steering

We are meeting to help develop and promote good practices in wellbore surveying necessary to support wellbore construction which enhance safety and competition. The meeting will be conducted in compliance with all laws including the antitrust laws, both state and federal. We will not discuss prices paid to suppliers or charged to customers nor will we endorse or disparage vendors or goods or services, divide markets, or discuss with whom we will or will not do business, nor other specific commercial terms, because these are matters for each company or individual to independently evaluate and determine.

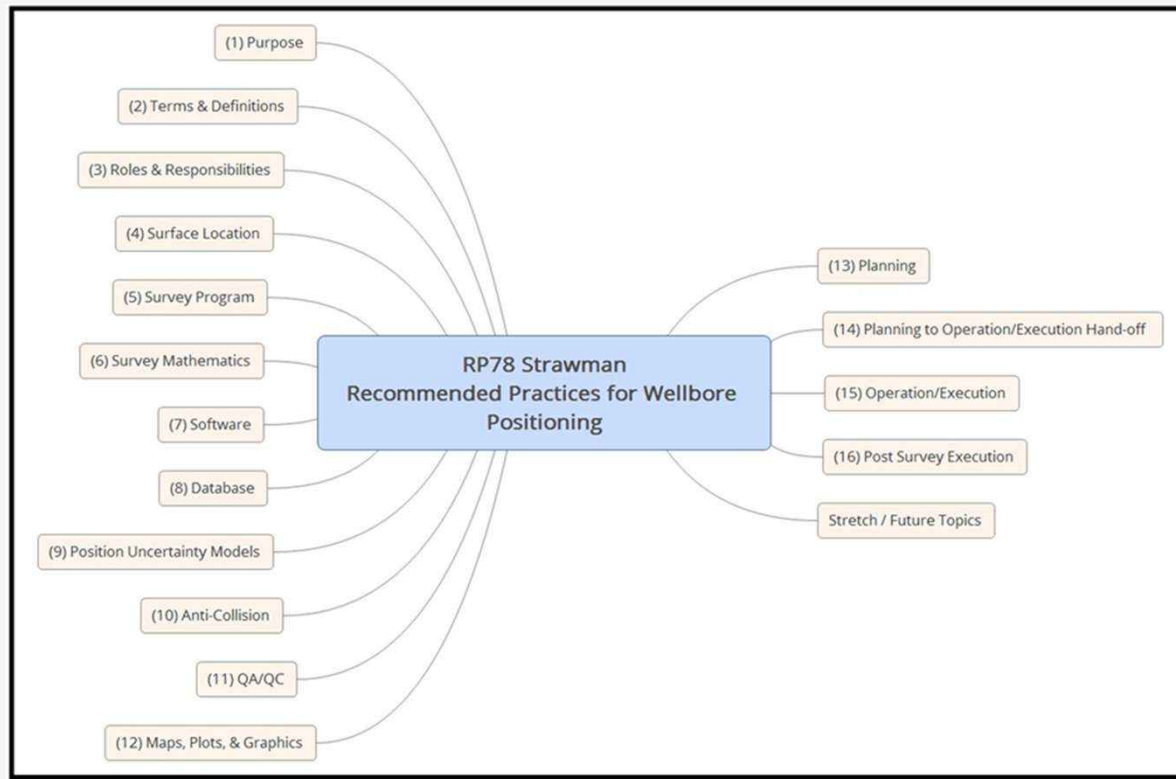
Virtual meetings are now held online every other month and

https://www.aade.org/download_file/4719/635

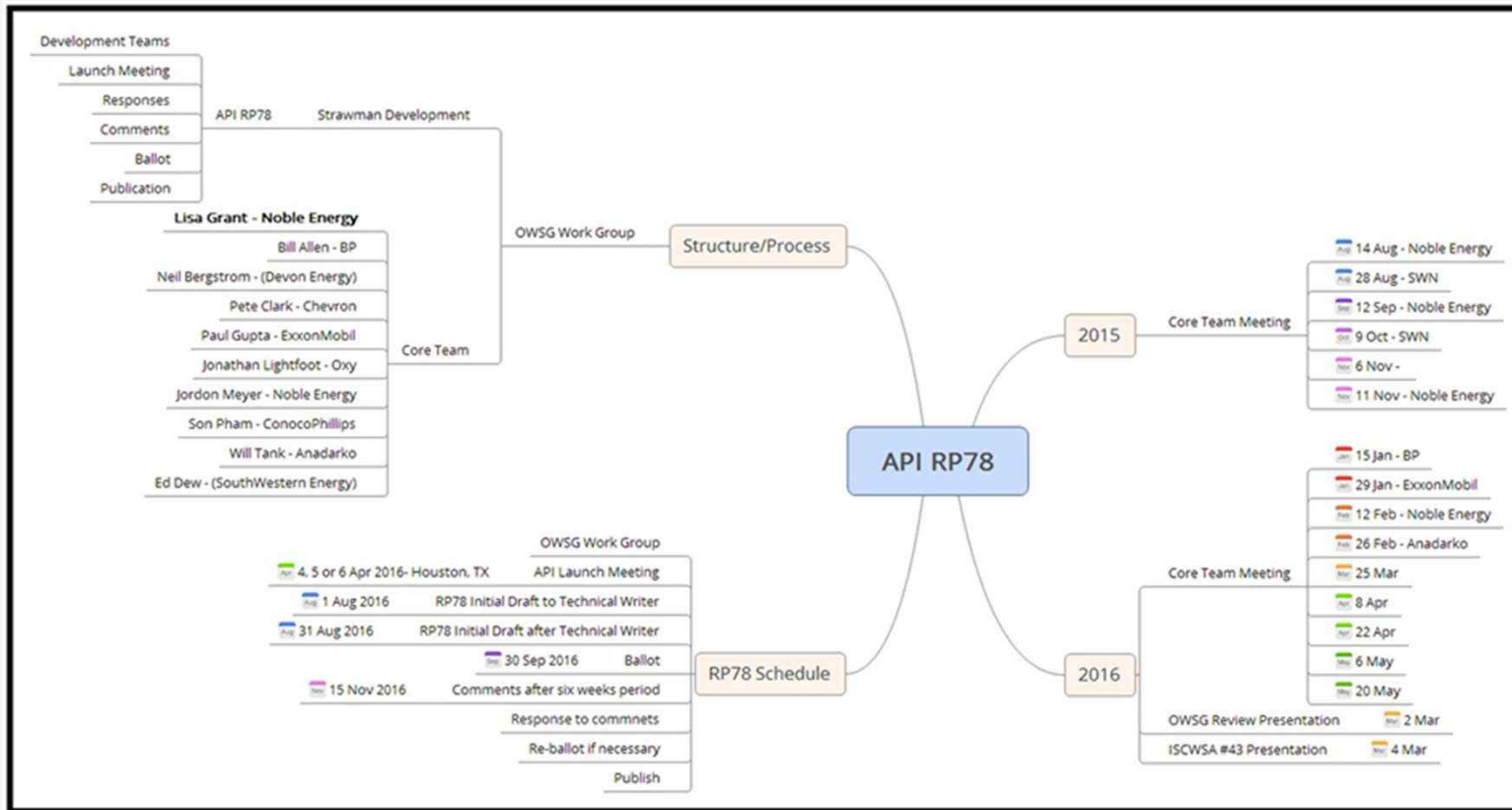
Published: April 4-5, 2023

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Overview: Original RP78 Strawman



Overview: Original RP78 Strawman



2025 BALLOT RESULTS



API Ballot Summary Sheet

Ballot: BALLOT: RP 78 Wellbore Surveying and Positioning

Ballot ID: 6610

Start Date: 2/13/2025

Closing Date: 3/27/2025

Associate: Jose Godoy

Coordinator: Jose Godoy

Proposal Review and comment on the first ballot for RP 78

Affirmative	Negative	Abstain	Did Not Vote
20	2	0	20

Total Responses: 22

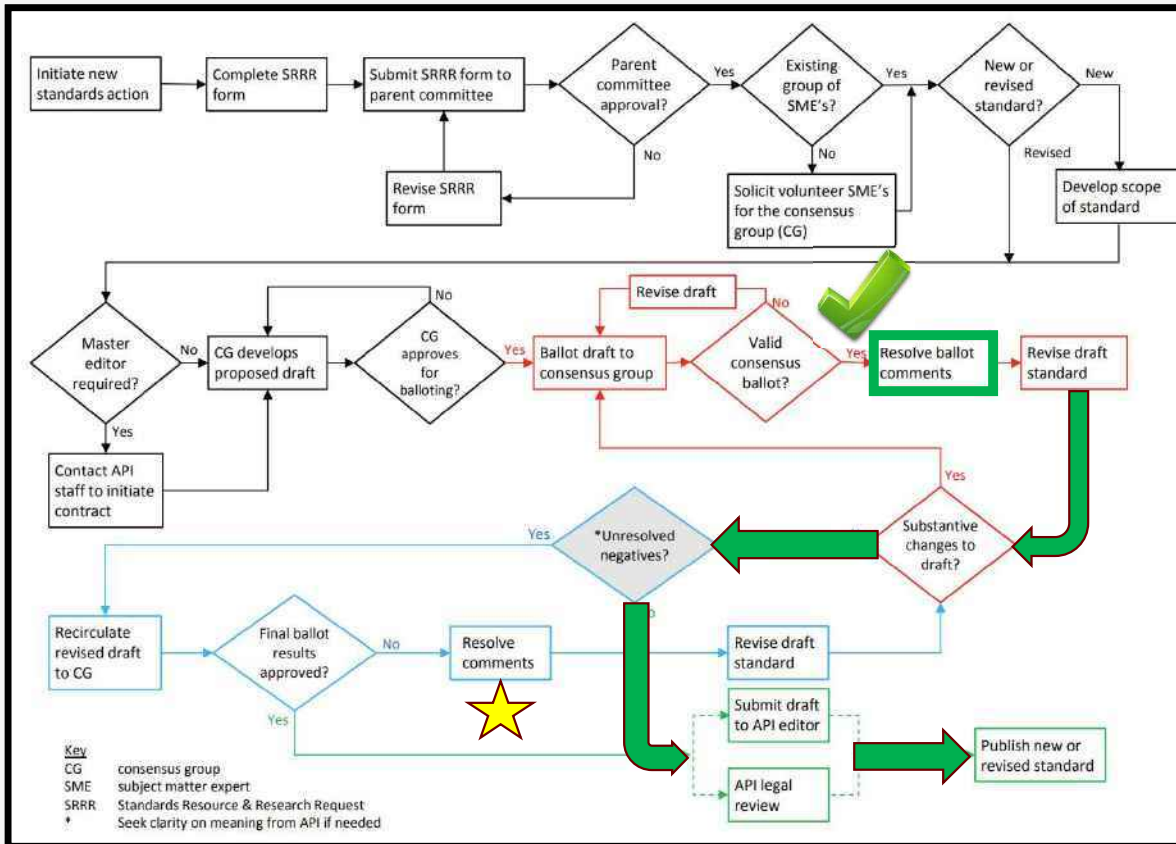
Total Ballots: 42

Response Rate = ((Affirmative + Negative + Abstain) / Total Ballots): **52.38%** Must be > 50%

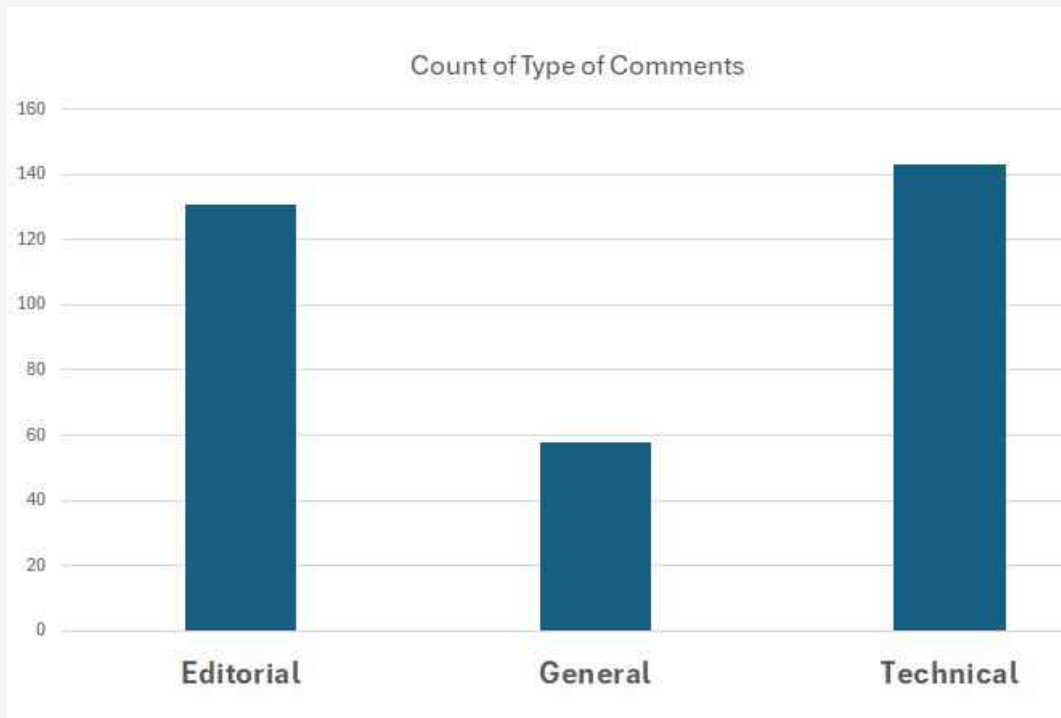
Approval Rate = (Affirmative / [Affirmative + Negative]): **90.91%** Must be >= 66.67%

Consensus: YES

API STANDARDS DEVELOPMENT PROCESS



BALLOT COMMENTS – QTY & TYPE



Comment Status	Comment Count
+ Accepted	47
+ Accepted in Principle	35
+ Not Accepted	5
+ Noted	11
+ (blank) Unresolved	234
Grand Total	332

Next steps

- **Update Draft Document to include Comment Edits**
- **Final Steps for the Comment Task Group**
 1. **Address Technical, General and Editorial Comments**
 2. **Finalize the Ballot Comment Draft**
 3. **Final Version Review by Comment Task Force**
 4. **API Technical Writer Review**
 5. **API Legal Review**
 6. **Final Copy Preparation**
 7. **Publish**

Questions?



WWW.API.ORG

WWW.ISCWSA.NET

WWW.SPE.ORG/WPTS

[AADE NTCE \(2023\)](#)